

## Response to Referees

### Sources and fate of nitrate in groundwater at agricultural operations overlying glacial sediments” by Sarah A. Bourke et al.

#### Referee #1

**1. General comments** It is interesting to assess the sources and fate of agriculturally derived NO<sub>3</sub>-N by the concentration of NO<sub>3</sub>-N and  $\hat{\sim} AL'CI \sim -$ . The idea of using  $f_d$  and  $f_m$  to quantify the impact of denitrification and dispersion are good. The tables and figures were displayed clearly and easy to understand.

*Thanks for taking the time to review, we are pleased that you saw value in the manuscript.*

**2. Specific comments** However, some specific scientific questions should be answered in this manuscript. Although the error in  $f_m$  introduced by neglecting  $Cl_b$  was discussed by authors, however, the error range may be underestimated. The largest error (calculated as 23% by authors) may be double as the  $Cl_b$  (assumed as 10 mg/L by authors)  $C1$  increased to 20 mg/L. The suggestion to improve this part in manuscript is to use an equation related to the ratio of  $Cl_b / Cl_i$ . I would also suggest to share the Excel sheet or program used by this manuscript. (page 6, line 35 to line 38).

*Our thanks to the reviewer for drawing our attention to this section of the manuscript; neglecting background concentrations was also raised by reviewer 2. The assumption that background concentrations can be neglected is a very useful simplifying assumption and is consistent with our understanding of the sites investigated. As such, we prefer to retain it in the final manuscript. Rather than altering the mathematical treatment, we have added a new figure (Figure 9) demonstrating that the influence of background concentrations on the calculated  $f_m$  is negligible in most cases. We have also updated the discussion around this assumption (see p14 of marked up manuscript).*

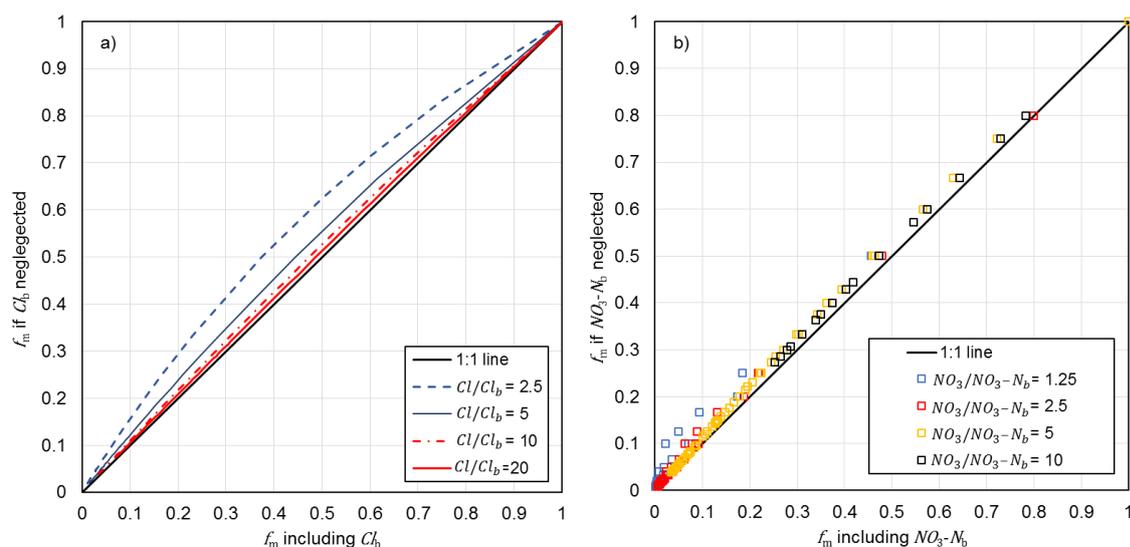


Figure 9 Effect of neglecting background concentrations ( $Cl_b$  or  $NO_3-N_b$ ) in the mixing model on calculated  $f_m$  over the range of values in this study.

*In lieu of an excel spreadsheet we have added a new table (Table S10) to the Supplementary Material outlining values of each of terms in the mixing model calculation for each sample. The only thing this Table doesn't include is the solver code in Excel, which is rudimentary.*

*Table S10 Constraining values and results of mixing model calculations*

Sample ID	Cl	NO <sub>3</sub> -N	$f_d$	NO <sub>3</sub> -N <sub>i</sub> /Cl <sub>i</sub>	Cl <sub>i</sub> (mg L <sup>-1</sup> )		NO <sub>3</sub> -N <sub>i</sub> (mg L <sup>-1</sup> )		$f_m$	
	(mg L <sup>-1</sup> )	(mg L <sup>-1</sup> )	(mean ± stdev)	(mean ± stdev)	min	max	min	max	min	max
<b>CFO1</b>										
DMW11	436.1	17.1	0.17 ± 0.07	0.23 ± 0.10	436	667	98	150	0.65	1
DMW12	78.0	2.6	0.23 ± 0.10	0.14 ± 0.06	78	1047	11	150	0.07	1
DMW13	56.7	23.7	0.56 ± 0.22	0.75 ± 0.29	57	189	42	141	0.30	1
DP10-2	74.5	11.8	0.52 ± 0.22	0.30 ± 0.13	74	277	23	84	0.27	1
DP11-12b	95.7	0.6	0.15 ± 0.08	0.04 ± 0.02	96	1300	4.2	90	0.07	1
DC15-22_10m	73.0	11.0	0.47 ± 0.21	0.32 ± 0.14	73	289	23	93	0.25	1
DP11-13_4.3m	28.5	7.0	0.30 ± 0.15	0.82 ± 0.41	29	184	23	150	0.15	1
DP11-13_5.2m	25.0	7.8	0.34 ± 0.13	0.91 ± 0.35	25	160	23	146	0.16	1
DP11-13_7m	72.3	12.0	0.27 ± 0.13	0.62 ± 0.30	72	244	45	150	0.30	1
DP11-13_7.9m	70.8	9.1	0.17 ± 0.09	0.76 ± 0.40	71	199	54	150	0.36	1
DP11-13_8.8m	81.7	11.0	0.32 ± 0.15	0.89 ± 0.42	82	323	39	150	0.25	1
<b>CFO4</b>										
BC4	163.1	35.1	0.37 ± 0.13	0.58 ± 0.20	163	258	95	150	0.63	1
BMW2	595.6	16.5	0.13 ± 0.06	0.21 ± 0.10	596	707	127	150	0.84	1
BMW5	131.2	12.9	0.34 ± 0.16	0.29 ± 0.14	131	520	38	150	0.25	1
BMW6	156.0	0.4	0.01 ± 0.01	0.26 ± 0.26	156	1300	0.4	150	0.12	1
BMW7	134.7	11.6	0.21 ± 0.11	0.41 ± 0.22	135	365	55	150	0.37	1

**3. Technical corrections** There are several technical corrections should be done before it can be published.

1)I notice that, the last paragraph of “introduction” belongs to “experimental site description” of “methodology”. (page 3, line 7 to line 20).

*We agree that Lines 8-15 on p3 are a description of the sites and these have been moved to the top of methods as a separate site description subsection (2.1 Experimental Sites). This new section contains an expanded description of these two study sites (see p4 of marked up manuscript).*

2)This manuscript didn't mention what is the sampling depth for the “water table wells” in the “methodology” section. To my understanding, there were little difference between groundwater monitor well and groundwater sampling well. Normally, the groundwater sampling well take water samples in a specific range of depths.

*The screen intervals of all wells are presented in Table 1 (cited p3 L25) along with a description of monitoring wells in 2.1.1. Table 1 reports total well depth and screen length along with the statement in the caption that all screens are at the bottom of the well – which allows the reader to easily determine screen depth for each well. We feel that this is an efficient way of presenting the data and would prefer to retain it in the manuscript.*

*The distinction between water table wells and piezometers is about the screen length and potential for the screen interval to include part of the unsaturated zone. For a water table well the screen interval is ~4 m (at these sites) and is screened so that water levels will be within the screen interval throughout seasonal or annual water table fluctuations. Piezometers are screened at discrete depths within the aquifer and in this study screen lengths were usually 0.5 m. The full length of these piezometers remains within the saturated zone at all times. This distinction is relatively standard within the North American hydrogeology community.*

*We provide this information for the benefit of readers, but once defining these terms simply refer to both as monitoring wells through-out the manuscript. We feel that this approach provides a good balance between providing detailed information if the reader desires it without unnecessarily complicating the text.*

**No change made**

3) Sampling frequency. I'm not sure if the sample frequency of the chloride and N species were high enough to draw the conclusion, since the sample sizes was less than 30 and standard deviation seems not low.

*The Cl and NO<sub>3</sub> concentrations were measured at monthly to quarterly sampling intervals over a period of approximately 5 years and adequately capture temporal variation (see Figures 3 and 5). However, the isotope data are effectively a snapshot in time and do not capture temporal variation. This was already noted in the text (p12 L40-P13 L2 of original manuscript).*

*A sample size of 30 (note that Cl and NO<sub>3</sub> data set is larger than this) is not unusually small for a study of nitrate in groundwater using isotopes. A brief survey of published papers yields: n= 16 (Mengis et al., 2001), n=29 (Mariotti et al., 1988), n = 24 (Durka et al., 1994).*

*It isn't entirely clear which conclusion(s) the reviewer thinks are not supported by the data. We acknowledge the limitations of the individual data sets, which is why the conclusions were drawn from a synthesised analysis of multiple lines of evidence that included the spatial and temporal distribution of NO<sub>3</sub> in groundwater and sources, the isotopic composition of that NO<sub>3</sub> and the mixing model results.*

*We believe that the conclusion that denitrification is proceeding in the groundwater system and that denitrification reduces NO<sub>3</sub> concentrations substantially at the farm-scale is strongly supported by the data. The attribution of sources has more uncertainty in it, but nonetheless, we feel that the spatial distribution of NO<sub>3</sub> as well as the mixing ratio analysis supports the conclusion that temporary piles and pens are equal or more significant sources of agricultural nitrate in groundwater at these sites.*

**No change made**

4)Text clarity. Section 3.1 and 3.2 mentioned several “water table wells” labeled as DMW11, DMW14, etc. However, it’s not easy for reader to look for those wells from figure 1 (the site description map)

*It’s not clear exactly what the issue is here. DMW11 is clearly visible at the top of Figure 1, DMW14 is clearly visible on the RHS of the inset (area covered delineated by blue rectangle as stated in caption), which is included specifically so that these closely spaced wells can be identified. If further guidance can be provided we have no problem making adjustments so that it is easier for the reader to understand. Perhaps just having the Figure 1 imbedded in the text rather than at the end of the manuscript will help?*

**No change made**

## **Referee #2**

This paper presents a study of using isotope (N15 and O18) to study the nitrate mixing and transport. Denitrification of nitrate was considered in this study. The authors argued that their study used isotope in a quantitative way, different from the qualitative way of previous study. This however seems an overstatement to me, because they only used the isotope data to calculate the mixing ratios and denitrification coefficients. This is not very quantitative.

*This manuscript presents the first application of the dual-isotopic enrichment of  $\text{NO}_3$  to quantify the fraction of  $\text{NO}_3$  removed that includes uncertainty in source values and enrichment factors. This type of calculation is commonly made using other isotopes, (e.g. calculating the amount of water lost to evaporation), but has not as yet been utilised in  $\text{NO}_3$  studies due to uncertainties in source values and enrichment factors. This is in stark contrast to the vast majority of published papers that used nitrate isotopes to identify the process of denitrification, or to define end-members for mixing calculations. We believe that this is a clear distinction and our analysis approach and results are correctly described as quantitative.*

*The text of the introduction has been extensively updated to clarify our approach and highlight the novel contribution of this manuscript to published literature (p2-3 marked up manuscript). We have also included an additional figure (Figure 8) that shows the reduction in  $\text{NO}_3\text{-N}$  concentrations associated with mixing and denitrification to emphasize the quantitative nature of our results, which is discussed in Section 3.4 of the revised manuscript.*

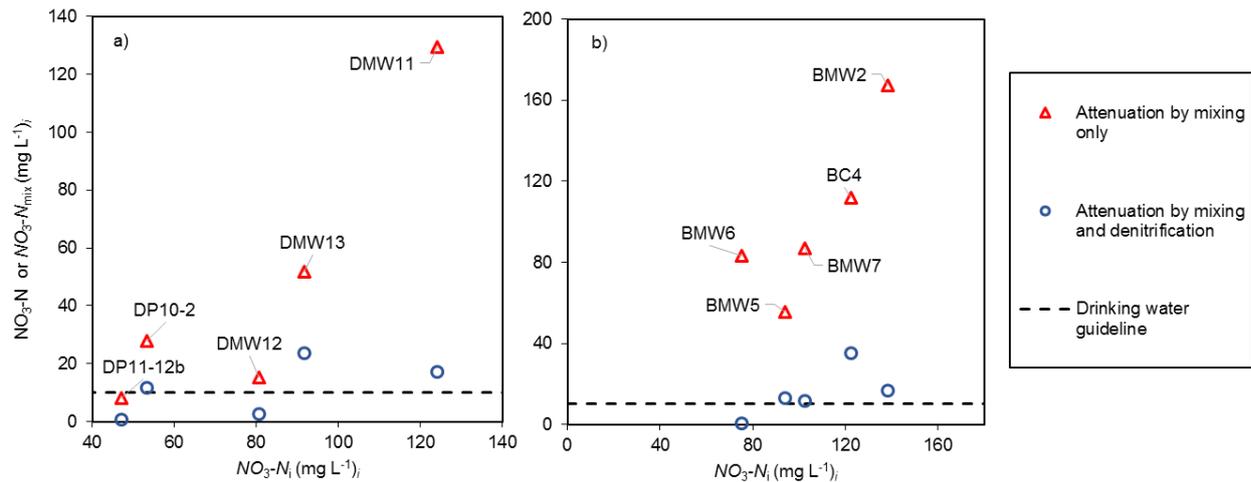


Figure 8 Measured concentrations of  $NO_3-N$  (blue circles - attenuation by mixing and denitrification) and  $NO_3-N_{mix}$  (red triangles - attenuation by mixing only) vs mid-range estimate of  $NO_3-N_i$  at a) CFO1 and b) CFO4. Dashed lines are drinking water guideline ( $10\text{ mg L}^{-1}$  of  $NO_3-N$ ).

I also have a few questions, listed below, related to their calculation of the mixing ratios and denitrification coefficients. The authors used in equation (4) of the two-member mixing method to calculate the nitrate mixing ratio. This does not seem right to me, because there should be more than C1 two nitrate sources, such as the background ambient groundwater, the direct infiltration from fertilizer, the manure source, and the transformation from ammonium to nitrate. I doubt that the two end-member method is adequate to consider the multiple sources.

*To the best of our knowledge (including interviews with long-time landowners/farmers at the sites, historic air photos) fertilizer (other than manure) has not been applied at the sites. As such, manure is the only source of agricultural nitrate at these study sites, which is stated in the original manuscript (p3 L13-15). This has now been clarified in the new subsection 2.1 (p4 marked up manuscript)*

*The nitrate in groundwater will have originally been organic-N or ammonium, and  $NH_3$  dominates N in the EMS at both sites. However, the data demonstrate that  $NH_3$  is generally a relatively small component of total-N in groundwater (<10%) so that  $NH_3$  can be neglected in the mixing model, which only considers the N-pool in the groundwater system. A new Table has been added (Table 2) that summarises the range of values of each of the components of the N-pool. Additional description of these values has also been added to the beginning of the Section 3.3 (p10 marked up manuscript).*

Table 2. Range of measured concentrations of TN,  $NH_3-N$ ,  $NO_x-N$  ( $NO_2-N + NO_3-N$ ) and TON at each study site. At CFO1 results from monitoring well DMW3 are presented separately because values in this well differed substantially from all other wells.

Site	N-pool	TN ( $\text{mg L}^{-1}$ )	$NH_3-N$ ( $\text{mg L}^{-1}$ )	$NO_x-N$ ( $\text{mg L}^{-1}$ )	TON ( $\text{mg L}^{-1}$ )
CFO1	EMS	550 – 1820	275 – 747	<0.1 – 0.4	73 – 1301
	Catch-basin	200 – 1440	2.5 – 7.3	<0.1	196 – 1437
	DMW3	278 – 548	219 – 479	<0.1 – 50 <sup>a</sup>	31.3 – 73.9
	Other monitoring wells	<0.25 – 33.4	<0.05 – 2.9	<0.1 – 31.4 <sup>**</sup>	<0.2 – 3.7
CFO4	EMS <sup>c</sup>	1000 – 1240	724 – 747	0.25 – 0.29	275 – 492
	Monitoring wells	<0.25 – 84.6	<0.05 – 0.23	<0.1 – 80.4	<0.2 – 13.9

<sup>a</sup>  $NO_x-N$  of  $50\text{ mg L}^{-1}$  in DMW3 consisted of  $12.6\text{ mg L}^{-1}$  as  $NO_3-N$  and  $37.4\text{ mg L}^{-1}$  as  $NO_2-N$ .

<sup>\*\*</sup>  $NO_x-N$  max in groundwater measured in core ( $NO_3-N = 66.4\text{ mg L}^{-1}$ ,  $NO_x-N = 67.8\text{ mg L}^{-1}$ )

<sup>c</sup> Range across three replicates measured on 25 August 2011

*At CFO4 ammonium concentrations in the groundwater system are negligible (consistently < 0.23 mg/L. At CFO1, well DMW3 directly adjacent to the EMS has NH<sub>3</sub> is present at high concentrations in and NO<sub>3</sub> concentrations were low, but the mixing calculation were not conducted on data from this well. In samples for which the mixing calculation was conducted NH<sub>3</sub> was <10% of total-N. This is now clearly stated in Section 2.4.2 (p7 of updated manuscript).*

*Also, NO<sub>2</sub> concentrations in groundwater at CFO1, which would be expected to be elevated in the presence of nitrification (Vogel et al., 1981), was consistently < 0.5 mg/L (see p12 L14-23 and Supplementary material). The one exception is core sample DP22\_6.5m, which has now been removed from the mixing calculation results (see updated Tables, Figures and text).*

*As such, we believe that it is reasonable to use a two-end member mixing model for the samples reported at these sites, where the end-members represent manure-based NO<sub>3</sub> and background (pre-agricultural) concentrations. This may not be the case at other sites where fertilizer or nitrification in groundwater are significant sources of NO<sub>3</sub> in groundwater, and this is now acknowledged in the Discussion (p14 marked-up manuscript).*

To account for the denitrification, the authors used a denitrification coefficient in equation (4). While this is conceptually OK, it does not consider that denitrification is a kinetic process (zeroth-order or first order). In other words, the denitrification coefficient used in the paper cannot reflect the kinetics of denitrification.

*In this study we assume that fractionation of NO<sub>3</sub> in groundwater during denitrification follows a Rayleigh distillation process, as described in Section 2.3.1. This approach has been used in numerous previously published studies of denitrification in groundwater (Böttcher et al., 1990; Otero et al., 2009; Xue et al., 2009) and these references are now clearly cited in the manuscript (see p6 marked up version).*

*Rates of denitrification are likely to vary, and this will be reflected in the enrichment factor (Kendall and Aravena, 2000). This leads to uncertainty in the enrichment factor, and is one of the reasons that dual-isotopic enrichment of NO<sub>3</sub> isn't widely quantified based from isotopic enrichment. This has now been clarified in the Introduction of the manuscript and in the description of the modelling approach.*

*In this study we determined a global epsilon of -10 based on data across both sites. In the model, epsilon values were allowed to vary in accordance with a normal distribution (mean = -10, stdev = -2.5), which will reflect a range of possible reaction rates. This value of epsilon was determined based on data measured at the site, as shown in Figure 2b. The slopes corresponding ± 1 std. dev. are now also shown on this Figure.*

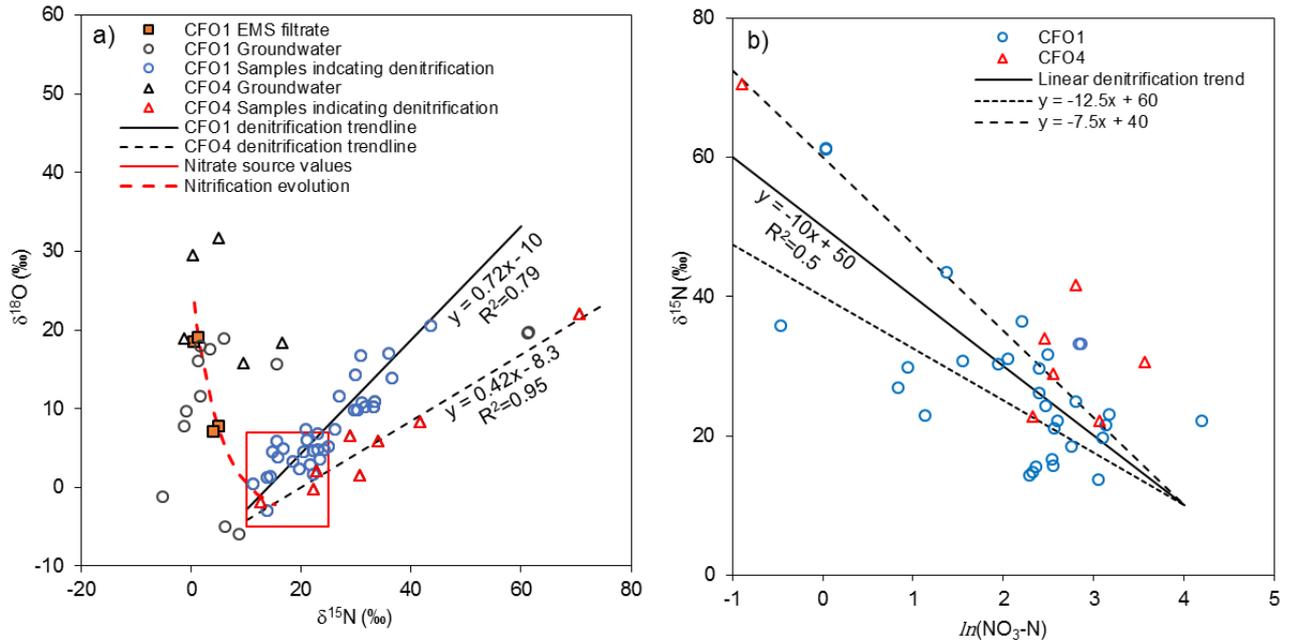


Figure 1 (a) Cross-plot of stable isotopes of nitrate at CFO1 and CFO4 showing hypothetical nitrification trend, boundary of manure-sourced  $\text{NO}_3^-$  values and linear enrichment trends associated with denitrification, (b) enrichment of  $\delta^{15}\text{N}_{\text{NO}_3}$  during denitrification (only samples within source region and with evidence of denitrification are shown) dashed lines represent  $\pm 1$  std. dev. of enrichment factor ( $\epsilon = -10$ ) estimated from measured data.

As to denitrification, it is unclear to what extent denitrification occurs in the aquifer. The plots in Figure 2 do not support the conclusion on denitrification, because the slopes shown in Figure 2(a) are not 0.5. For well CFO4, the slope of 0.42 is close to 0.5m, and the data listed in Table 2 and the well locations shown in Figure 1 indeed support the conclusion of denitrification. But what about well CFO1?

*We assume that the reviewer takes issue with the slope of the isotopic enrichment trend at CFO1 (0.72) as being not close enough to the general trend of 0.5 reported in some studies (Durka et al., 1994). However the value of 0.72 is not unreasonable given the range of values reported for denitrification of groundwater in the published literature of 0.47 – 0.66 (Singleton et al., 2007), 0.67 (Mengis et al., 1999), 0.77 (Fukada et al., 2003). This will have now been clarified in the description of the modelling approach.*

The authors said somewhere in the manuscript that the initial nitrate concentration can be neglected. I do not think that it is a reasonable assumption for agricultural areas.

*Presumably the reviewer is suggesting that there can be an historical legacy of nitrate in agricultural areas. This is true, and we consider “background” as not having been influenced by agricultural activity (whether this is recent or historical). This assumption that  $\text{NO}_{3b}$  can be neglected underpins the simplification of the mathematics and is valid for these agricultural areas. This approach would not be suitable at sites with naturally elevated nitrate concentrations in groundwater, which is now acknowledged in the manuscript.*

*A new figure (Figure 8, see above response to reviewer 1) has been added to the revised manuscript to demonstrate that the effect of neglecting background concentrations at these sites is negligible, and discussion of the effect of neglecting background concentrations has been updated.*

## **References**

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# Sources and fate of nitrate in groundwater at agricultural operations overlying glacial sediments

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10 **Abstract.** Leaching of nitrate ( $\text{NO}_3^-$ ) from animal waste or fertilizers at agricultural operations can result in  $\text{NO}_3^-$  contamination of groundwater, lakes, and streams. Understanding the sources and fate of nitrate in groundwater systems in glacial sediments, which underlie many agricultural operations, is critical for managing impacts of human food production on the environment. Elevated  $\text{NO}_3^-$  concentrations in groundwater can be naturally attenuated through mixing or denitrification. Here we use ~~snapshots~~isotopic enrichment of the stable isotope values of  $\text{NO}_3^-$  to quantify the amount of denitrification in groundwater at two confined feeding operations overlying glacial sediments in Alberta, Canada. Uncertainty in  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  values of the  $\text{NO}_3^-$  source and denitrification enrichment factors are accounted for using a Monte Carlo approach. When denitrification could be quantified, we ~~reconstructed~~used these values to constrain a mixing model based on  $\text{NO}_3^-$  and  $\text{Cl}^-$  concentrations. Using this novel approach we were able to reconstruct the initial  $\text{NO}_3\text{-N}$  concentration and  $\text{NO}_3\text{-N}/\text{Cl}^-$  ratio at the point of entry to the groundwater system. The addition of  $\text{NO}_3^-$  to the local groundwater system from temporary manure piles and pens equalled or exceeded  $\text{NO}_3^-$  additions due to leaching from earthen manure storages at these sites. As such, on-farm management of manure waste to limit  $\text{NO}_3^-$  contamination of groundwater should increasingly focus on limiting manure piles in direct contact with the soil, and encourage storage in lined lagoons. Nitrate attenuation at both sites is attributed to a spatially variable combination of mixing and denitrification, but is dominated by denitrification. On-site denitrification reduced agriculturally derived  $\text{NO}_3^-$  concentrations by at least half and, in some wells, completely. ~~These results indicate that~~Therefore, infiltration to groundwater systems in glacial sediments where  $\text{NO}_3^-$  can be naturally attenuated is likely preferable to off-farm export via runoff or drainage networks. ~~The application of isotopes of nitrate to constrain a mixing model based on concentrations of  $\text{Cl}^-$  and  $\text{NO}_3^-$ , which can be routinely monitored in groundwater, provides a relatively simple method to assess the sources and fate of agriculturally derived  $\text{NO}_3^-$  in these settings., if local groundwater is not used for potable water supply.~~

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## 1 Introduction

The contamination of soil and groundwater with nitrate from agricultural operations is a global water quality issue that has been extensively documented (Power and Schepers, 1989; Spalding and Exner, 1993; Rodvang and Simpkins, 2001; Galloway et al., 2008; Zirkle et al., 2016; Arauzo, 2017; Ascott et al., 2017). Leaching of nitrate ( $\text{NO}_3^-$ ) from animal waste or fertilizers can result in groundwater  $\text{NO}_3^-$  concentrations that exceed drinking water

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guidelines and pose human health risks (Fan and Steinberg, 1996; Gulis et al., 2002; Yang et al., 2007). The discharge of high-NO<sub>3</sub><sup>-</sup> groundwater, runoff, or drainage can contaminate streams and lakes, resulting in eutrophication and ecosystem decline (Deutsch et al., 2006; Kaushal et al., 2011). In saturated groundwater systems with low oxygen concentrations, elevated NO<sub>3</sub><sup>-</sup> can be naturally attenuated by microbial denitrification (Wassenaar, 1995; Robertson et al., 1996; Smith et al., 1996; Tesoriero et al., 2000; Singleton et al., 2007). Concentrations of NO<sub>3</sub><sup>-</sup> will also decrease along groundwater flow paths due to attenuation via dilution by hydrodynamic dispersion (referred to hereafter as mixing). Because of these natural attenuation mechanisms, infiltration to groundwater may be preferable to off-site drainage and runoff of nitrate-rich waters. Many agricultural operations are undertaken on fertile soils associated with glacial sediments (Spalding and Exner, 1993; Ernstsens et al., 2015; Zirkle et al., 2016). Understanding the sources and fate of agriculturally derived nitrate in groundwater systems in glacial sediments is therefore critical for managing impacts of human food production on the environment.

Identification of the sources and fate of NO<sub>3</sub><sup>-</sup> at agricultural operations can be challenging because of spatial and temporal variations in sources (e.g. earthen manure storage, temporary manure piles, or fertilizer) and the complexity of hydrogeologic systems (Spalding and Exner, 1993; Rodvang et al., 2004; Showers et al., 2008; Kohn et al., 2016). These spatial and temporal variations can result in complex subsurface solute distributions that are difficult to interpret using classical transect studies or numerical groundwater models (Green et al., 2010; Baily et al., 2011).

Groundwater containing significant agriculturally derived NO<sub>3</sub><sup>-</sup> also typically has elevated chloride (Cl<sup>-</sup>) concentrations (Saffigna and Keeney, 1977; Rodvang et al., 2004; Menció et al., 2016). Decreasing NO<sub>3</sub>-N/Cl<sup>-</sup> (or NO<sub>3</sub><sup>-</sup>/Cl<sup>-</sup>) ratios have been used to define denitrification based on the assumption that NO<sub>3</sub><sup>-</sup> is reactive while Cl<sup>-</sup> is non-reactive (conservative), such that denitrification results in a decrease in the NO<sub>3</sub>-N/Cl<sup>-</sup> ratio (Kimble et al., 1972; Weil et al., 1990; Liu et al., 2006; McCallum et al., 2008). However, NO<sub>3</sub>-N/Cl<sup>-</sup> ratios can also change in response to mixing of groundwater with different NO<sub>3</sub>-N/Cl<sup>-</sup> ratios or when groundwater sampling traverses hydraulically disconnected formations (Bourke et al., 2015b). If NO<sub>3</sub>-N/Cl<sup>-</sup> ratios vary among potential sources and the NO<sub>3</sub>-N/Cl<sup>-</sup> ratio at the point of entry to the groundwater system can be reconstructed, this information could be used to show that anthropogenic NO<sub>3</sub><sup>-</sup> at different locations within an aquifer is derived from the same or different sources.

The stable isotopes of NO<sub>3</sub><sup>-</sup> ( $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$ ) provide an alternative approach to characterize the source and fate of NO<sub>3</sub><sup>-</sup> in groundwater systems. In agricultural areas, multiple sources of NO<sub>3</sub><sup>-</sup> are common and could include precipitation, soil NO<sub>3</sub><sup>-</sup>, inorganic fertilizer, manure, and septic waste (Komor and Anderson, 1993; Liu et al., 2006; Pastén-Zapata et al., 2014; Clague et al., 2015; Xu et al., 2015). While source identification is theoretically possible using  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  (particularly with a dual-isotope approach), in practice this can be difficult due to geologic heterogeneity, overlapping source values, and the complexity of biologically mediated reactions (Aravena et al., 1993; Wassenaar, 1995; Mengis et al., 2001; Choi et al., 2003; Granger et al., 2008; Vavilin and Rytov, 2015; Xu et al., 2015). NO<sub>3</sub><sup>-</sup> attenuation by denitrification in groundwater systems can be identified based on the characteristic enrichment of  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$ . Numerous studies have made qualitative assessments of that identified denitrification in groundwater using the stable isotope approach (Böttcher et al., 1990; Wassenaar, 1995; Singleton et al., 2007; Baily et al., 2011; Clague et al., 2015; Xu et al., 2015). ~~However, very few~~ Recently published ~~field studies report quantitative assessments of denitrification based on~~ papers have also used stable

isotopic enrichment values of  $\delta^{15}\text{N}_{\text{NO}_3^-}$  and  $\delta^{18}\text{O}_{\text{NO}_3^-}$  and, to our knowledge, none account water as the basis for uncertainties in mixing models in agricultural settings (Ji et al., 2017; Lentz and Leheresch, 2019). Isotopic fractionation effects can also allow for quantitative assessment of the proportion of substrate that has undergone a given reaction, if enrichment factors and source values are known; as in the case of evaporative loss of water, for example (Dogramaci et al., 2012). To date, there have been very few attempts to quantify denitrification using dual-isotope enrichment, largely due to uncertainty in source values and enrichment factors (Böttcher et al., 1990; Otero et al., 2009; Xue et al., 2009).

The only published calculations of the fraction of  $\text{NO}_3^-$  remaining after denitrification that we are aware of assumed a constant enrichment factor and the same isotopic source values across the field site (Otero et al., 2009). However, the enrichment factor will vary across a field site in response to reaction rates (Kendall and Aravena 2000), and isotopic values of even the same type of source (e.g. manure) can vary substantially (Xue et al., 2009). If the variation in source values and enrichment factors can be characterized from measured data then these uncertainties can be accounted for using a Monte Carlo approach (Joerin et al., 2002; Bourke et al., 2015a; Ji et al., 2017), thereby extending the application of the dual-isotope technique to allow for a robust quantitative assessment of denitrification in agricultural settings.

A synthesized analysis of stable isotopes of  $\text{NO}_3^-$  with additional ionic tracers can further improve the assessment of  $\text{NO}_3^-$  attenuation mechanisms and sources of  $\text{NO}_3^-$  in agricultural settings (Showers et al., 2008; Vitòria et al., 2008; Xue et al., 2009; Xu et al., 2015). If, Ji et al., 2017). We hypothesise that if the amount of denitrification can be quantified based on  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$ , then this estimate of the fraction of  $\text{NO}_3\text{-N}$  removed through denitrification can be used to constrain a mixing model based on  $\text{NO}_3\text{-N}$  and  $\text{Cl}^-$  concentrations. This novel approach allows for the ratio of  $\text{NO}_3\text{-N}/\text{Cl}^-$  at the point of entry to the groundwater system ~~can be calculated/reconstructed~~ from measured  $\text{NO}_3^-$  and  $\text{Cl}^-$  concentrations (see Section 2.3) and this). Where the  $\text{NO}_3\text{-N}/\text{Cl}^-$  ratio varies between sources, this ratio can then be used to assess the source of the  $\text{NO}_3^-$  in groundwater (e.g. temporary manure piles or feeding pens). These data can also then be used to quantify attenuation by mixing and estimate the initial concentrations of  $\text{NO}_3^-$  and  $\text{Cl}^-$  at the point of entry to the groundwater system. ~~Uncertainties in source values and enrichment factors can be constrained using measured data and explicitly and quantify attenuation by mixing, accounted for using a Monte Carlo approach (Joerin et al., 2002; Bourke et al., 2015a).~~

In this study, we present the application of this approach at two confined feeding operations (CFOs) in Alberta, Canada, with differing lithologies and durations of operation (Fig. 1). The first study area (CFO1), located 25 km northeast of Lethbridge, Alberta, was established in 1928 and had approximately 150 head of dairy cattle at the time of the study. An associated earthen manure storage (EMS) facility for storing liquid dairy manure was constructed in the 1960s. A 2000 head beef feedlot, established in the 1960s, was also present at CFO1. The second study area (CFO4), located approximately 30 km north of Red Deer, Alberta and 300 km north of CFO1, was constructed in 1995 (including an EMS) and had 350 head of dairy cattle at the time of the study. To the best of our knowledge, fertilizers have not been applied at either of these sites, and infiltration of manure waste is assumed to be the cause of elevated  $\text{NO}_3^-$  concentrations in the local groundwater. Concentrations of  $\text{Cl}^-$  and nitrogen species (N-species) and the stable isotopes of  $\text{NO}_3^-$  were measured in groundwater samples collected from monitoring wells and continuous soil cores, as well as manure filtrate at both sites. These data were interpreted to (1) assess the extent of agriculturally derived  $\text{NO}_3^-$  in groundwater, (2) identify sources and initial

concentrations of  $\text{NO}_3^-$  at the point of entry to the groundwater system, and (3) assess the dominant attenuation mechanisms controlling subsurface  $\text{NO}_3^-$  distributions at these sites.

## 2 Materials and methods

### 2.1 Experimental sites

5 This study was conducted using data from two of the five sites investigated by Alberta Agriculture and Forestry during an assessment of the impacts of livestock manure on groundwater quality (Lorenz et al., 2014). To the best of our knowledge (including discussions with farm operators) fertilizers have not been applied at either of these sites. As such, manure waste from livestock is assumed to be the sole source of agricultural nitrogen (N) and elevated  $\text{NO}_3^-$  concentrations in groundwater at these sites.

10 The first study site (CFO1) is located 25 km northeast of Lethbridge, Alberta (Fig. 1). Agricultural operations at this site were initiated with the construction of a dairy in 1928, with the capacity for the 150 dairy cattle since the 1960s. A feedlot for beef cattle was added in 1960s along with an earthen manure storage (EMS) facility for storing liquid dairy manure (approx. 4 m deep) and a catch-basin that receives surface water runoff. This feedlot was expanded in the 1980s to the 2000 head capacity it was at the time of this study. There is also a dugout (or slough, a shallow wetland) on site that receives local runoff and an irrigation drainage canal at the southern boundary of the property.

15 The second study site (CFO4) is located approximately 30 km north of Red Deer, Alberta and 300 km north of CFO1. This dairy and associated EMS (approx. 6 m deep) were constructed in 1995 and the facility had 350 head of dairy cattle at the time of the study. Runoff will drain either to the small dugout in the north-west of the site, or  
20 the natural drainage features (ephemeral ponds or a creek approx. 1.5 km east).

### 2.2 Sampling and instrumentation

#### 2.2.1 Groundwater monitoring wells

Groundwater samples were collected from water table wells and piezometers (hereafter both are referred to as wells) installed at both sites (Fig. 1, Table 1). At CFO1, groundwater samples were collected from six individual  
25 water table wells (DMW1, DMW2, DMW3, DMW4, DMW5, DMW6) and eight sets of nested wells with one well screened at the water table and one well screened 20 m below ground (BG) (DP10-2 and DP10-1, DMW10 and DP11-10b, DMW11 and DP11-11b, DMW12 and DP11-12b, DMW13 and DP11-13b, DMW14 and DP11-14b, DMW15 and DP11-15b, and DMW16 and DP11-16b). Wells DP10-2 and DP10-1 were located directly adjacent to the EMS on the hydraulically downgradient side. At CFO4, groundwater samples were collected from  
30 eight water table wells (BC1, BC2, BC3, BC4, BC5, BMW1, BMW3, BMW7) and four sets of nested wells, with wells screened across the water table and at 15 m BG. Two of these nests were located adjacent to the EMS (BMW2 and BP10-15e, BMW4 and BP10-15w) and two were hydraulically downgradient of the EMS (BMW5 and BP5-15, BMW6 and BP6-15).

Groundwater samples were collected for ion analysis ( $\text{Cl}^-$  and N species) quarterly between April 2010 and August  
35 2015. All water samples were collected using a bailer after purging (1–3 casing volumes) and stored at  $\leq 4^\circ\text{C}$  prior to analysis. Samples for  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  were collected from wells at CFO1 on 1 January 2013 and 1 May 2013. Samples for  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  at CFO4 were collected on 27 October 2014. Wells were purged

prior to sample collection (1–3 casing volumes), and samples filtered into high-density polyethylene (HDPE) bottles in the field and frozen until analysis.

Hydraulic heads in monitoring wells were determined using manual measurements (approximately monthly, 2010-2015). Rising head response tests (slug or bail tests) were conducted to determine hydraulic conductivity (K) of the formation media surrounding the intake zone on the majority of the wells at the sites.

### 2.12.2 Continuous core

Continuous core was collected at CFO1 immediately adjacent to well DP11-13b on 1 May 2013 (Fig. 1). Additional core samples were collected from 1 to 5 June 2015 along a transect hydraulically downgradient of the southeastern side of the EMS at CFO1 where hydrochemistry data suggested leakage from the EMS (see Section 3). During this 2015 drilling campaign, core samples were collected at four locations (DC15-20, DC15-21, DC15-22, DC15-23) to depths of up to 15 m below surface and distances of up to 100 m from the EMS between wells DMW3 and DP11-14.

Continuous core samples were retrieved using a hollow stem auger (1.5-m core lengths) with 0.3-m sub-samples collected at approximately 1-m intervals ensuring that visually consistent lithology could be sampled. Core samples for Cl<sup>-</sup> were stored in Ziploc™ bags and kept cool until analysis. Core samples for N-species analysis were stored in Ziploc bags filled with an atmosphere of argon (99.9% Ar) to minimize oxidation and kept cool until analysis. Subsamples of each core (250-300 g) were placed under 50 MPa pressure in a Carver Series NE mechanical press with a 0.5- $\mu$ m filter placed at the base of the squeezing chamber, which was placed within an Ar atmosphere to minimize oxidation. A syringe was attached to the base of the apparatus and 15 mL of filtered pore water were collected for analyses within 3.5 to 6.0 h (Hendry et al., 2013).

### 2.12.3 Liquid manure storages

Samples of liquid manure slurry were collected directly from the EMS at both sites and the catch basin (containing local runoff from the feedlot) at CFO1 using a pipe and plunger apparatus to sample from approximately 0.5 m below the surface. The slurry collected was subsequently filtered (0.45  $\mu$ m) to separate the liquid and solid components. The water filtered from samples collected from the EMS or catch basin is hereafter referred to as manure filtrate.

### 2.23 Laboratory analysis

For groundwater samples from wells and manure filtrate, concentrations of Cl<sup>-</sup> were determined using potentiometric titration of H<sub>2</sub>O, with a detection limit of 5.0 mg L<sup>-1</sup> and accuracy of 5% (APHA 4500-Cl<sup>-</sup> D). Concentrations of NH<sub>3</sub> as N (NH<sub>3</sub>-N), NO<sub>3</sub><sup>-</sup> as N (NO<sub>3</sub>-N), and NO<sub>2</sub><sup>-</sup> as N (NO<sub>2</sub>-N) in groundwater samples from wells and manure filtrate were measured by air-segmented continuous flow analysis (APHA 4500-NH<sub>3</sub> G, APHA 4500-NO<sub>3</sub>- F). Total nitrogen (TN) was determined by high temperature catalytic combustion and chemiluminescence detection using a Shimadzu TOC-V with attached TN unit (ASTM D8083-16). Total Kjeldahl organic nitrogen (TKNTON) was ~~then~~ calculated by subtracting ~~the concentrations of~~ NH<sub>3</sub>-N, NO<sub>3</sub>-N and NO<sub>2</sub>-N from TN. Bicarbonate (HCO<sub>3</sub><sup>-</sup>) was analyzed by titration (APHA 2320 B). Dissolved organic carbon (DOC) was analyzed by a combustion infrared method (APHA 5310 B) using a Shimadzu TOC-V system.

Pore-water samples squeezed from continuous core were analyzed for  $\text{Cl}^-$ ,  $\text{NO}_3^-$ -N, and  $\text{NO}_2^-$ -N using a Dionex IC25 ion chromatograph (IC) coupled to a Dionex As50 autosampler (EPA Method 300.1, accuracy and precision of 5.0%) (Hautman and Munch, 1997). Ammonia as N ( $\text{NH}_3$ -N) was measured by Exova Laboratories using the automated phenate method (APHA Standard 4500-NH<sub>3</sub> G, detection limit of 0.025 mg L<sup>-1</sup>, accuracy of 2% of the measured concentration, and a precision of 5% of the measured concentration).

$\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  in groundwater samples (from wells and pore water from continuous core) and manure filtrate were measured at the University of Calgary (Calgary, Alberta) using the denitrifier method (Sigman et al., 2001) with an accuracy and precision of 0.3‰ for  $\delta^{15}\text{N}_{\text{NO}_3}$  and 0.3‰ for  $\delta^{18}\text{O}_{\text{NO}_3}$ . Groundwater samples collected for  $\text{NO}_3^-$  isotope analysis in January 2013 were also analyzed for  $\text{NO}_3^-$ -N by the University of Calgary (denitrifier technique, Delta+XL).

## 2.34 Modelling approach

### 2.34.1 Quantification of denitrification based on $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$

~~Groundwater Nitrate in groundwater~~ that has undergone denitrification ~~can be~~ commonly reported as being identified by enrichment of  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  with a ~~characteristic~~ slope of about 0.5 on a cross-plot (Clark and Fritz, 1997). ~~However, published studies of denitrification in groundwater report slopes of up to 0.77 (Mengis et al., 1999; Fukada et al., 2003; Singleton et al., 2007).~~ The relationship between isotopic enrichment of  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  and the fraction of  $\text{NO}_3^-$ -N remaining during denitrification can be described by a Rayleigh equation:

$$R = R_0 f_d^{\left(\frac{1}{\beta} - 1\right)}, \quad (1)$$

where  $R_0$  is the initial isotope ratio of the  $\text{NO}_3^-$  ( $\delta^{18}\text{O}_{\text{NO}_3}$  or  $\delta^{15}\text{N}_{\text{NO}_3}$ ),  $R$  is the isotopic ratio when fraction  $f_d$  of  $\text{NO}_3^-$  remains, and  $\beta$  is the kinetic fractionation factor ( $> 1$ ) (Böttcher et al., 1990; Clark and Fritz, 1997; Otero et al., 2009; Xue et al., 2009). Kinetic fraction effects are commonly also expressed as the enrichment factor,  $\varepsilon = 1000(\beta - 1)$ . In the case of a constant enrichment factor,  $f_d$  can be calculated from:

$$f_d = \exp\left(\frac{R - R_0}{\varepsilon}\right) \quad (2)$$

~~The extent of denitrification, as indicated by and~~ the fraction of  $\text{NO}_3^-$ -N remaining ~~(removed from groundwater through denitrification is given by  $(1 - f_d)$ ).~~ The concentration of  $\text{NO}_3^-$ -N that would have been measured if mixing was ~~quantified in the only attenuation mechanism ( $\text{NO}_3^-$ - $N_{\text{mix}}$ ) can also be calculated by dividing the measured concentration by  $f_d$ .~~

~~A~~ sub-set of 20 samples with isotopic values of  $\text{NO}_3^-$  indicative of denitrification. ~~For~~ were identified, and for each ~~sample, of these samples~~  $f_d$  (mean and standard deviation) was calculated from Eq. (2) using a Monte Carlo approach with 500 realizations. The value of  $R$  was given by the measured isotopic ratio for each sample ( $\delta^{18}\text{O}_{\text{NO}_3}$  or  $\delta^{15}\text{N}_{\text{NO}_3}$ ).  $R_0$  was allowed to vary randomly within a range of values determined from measured data and literature values. If the initial  $\delta^{15}\text{N}_{\text{NO}_3}$  is known,  $\varepsilon$  for  $\delta^{15}\text{N}_{\text{NO}_3}$  ( $\varepsilon_{15\text{N}}$ ) can be determined from the slope of the linear regression line on a plot of  $\ln(f_d)$  vs.  $\delta^{15}\text{N}_{\text{NO}_3}$  (Böttcher et al., 1990). If the initial  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $f_d$  are not known, as is the case here,  $\varepsilon_{15\text{N}}$  can be determined from the slope of the regression line on a plot of  $\ln(\text{NO}_3^- \text{-N})$  vs.  $\delta^{15}\text{N}_{\text{NO}_3}$ , which will be the same as on a plot of  $\ln(f_d)$  vs.  $\delta^{15}\text{N}_{\text{NO}_3}$ . ~~In-situ variations in temperature and reaction rates may affect the enrichment factor (Kendall and Aravena, 2000) and this was accounted for by allowing for variation in  $\varepsilon_{15\text{N}}$  within the Monte Carlo analysis.~~ The enrichment factor for  $\delta^{18}\text{O}_{\text{NO}_3}$  ( $\varepsilon_{18\text{O}}$ ) was calculated by multiplying the  $\delta^{15}\text{N}_{\text{NO}_3}$  by a linear coefficient of proportionality determined for each CFO from the slope of the denitrification

trend on an isotope cross-plot (see Section 3.2). This approach neglects the effect of mixing of groundwater with differing isotopic values, and is valid if the concentration of  $\text{NO}_3^-$  in the source is much greater than background concentrations such that the isotopic composition of  $\text{NO}_3^-$  is dominated by the agriculturally derived end-member.

### 2.34.2 Quantification of mixing and initial concentrations of $\text{Cl}^-$ and $\text{NO}_3\text{-N}$

5 A binary mixing model that also accounts for decreasing  $\text{NO}_3\text{-N}$  concentrations in response to denitrification was used to quantify  $\text{NO}_3^-$  attenuation by mixing and estimate the initial concentrations of  $\text{Cl}^-$  and  $\text{NO}_3\text{-N}$ . The measured concentration of  $\text{Cl}^-$  was assumed to be a function of two end-member mixing, described by

$$Cl = f_m Cl_i + (1 - f_m) Cl_b, \quad (3)$$

10 where  $Cl$  is the measured concentration of  $\text{Cl}^-$  in the groundwater sample,  $Cl_i$  is the concentration of  $\text{Cl}^-$  at the initial point of entry of the agriculturally derived  $\text{NO}_3^-$  to the groundwater system,  $Cl_b$  is the concentration of  $\text{Cl}^-$  in the background ambient groundwater, and  $f_m$  is the fraction of water in the sample from the source of agriculturally derived  $\text{Cl}^-$  (and  $\text{NO}_3^-$ ) remaining in the mixture.

The concentration of  $\text{NO}_3\text{-N}$  was also assumed to be a function of two end-member mixing but with an additional coefficient,  $f_d$  (the fraction of  $\text{NO}_3\text{-N}$  remaining after denitrification), applied to account for denitrification. The measured  $\text{NO}_3\text{-N}$  concentration was thus described by

$$\text{NO}_3\text{-N} = f_d (f_m \text{NO}_3\text{-N}_i + (1 - f_m) \text{NO}_3\text{-N}_b), \quad (4)$$

15 where  $\text{NO}_3\text{-N}$  is the concentration of  $\text{NO}_3\text{-N}$  measured in the groundwater sample,  $\text{NO}_3\text{-N}_i$  is the concentration of  $\text{NO}_3\text{-N}$  in the source of agriculturally derived  $\text{NO}_3^-$  at the initial point of entry to the groundwater system, and  $\text{NO}_3\text{-N}_b$  is the concentration of  $\text{NO}_3\text{-N}$  in the background ambient groundwater. This mixing calculation was only conducted on samples for which  $\text{NO}_3^-$  dominated total-N ( $\text{NH}_3\text{-N} < 10\%$  of  $\text{NO}_3\text{-N}$ ) so that nitrification of  $\text{NH}_3$  could be neglected.

If  $Cl_i$  is much greater than  $Cl_b$  and  $\text{NO}_3\text{-N}_i$  is much greater than  $\text{NO}_3\text{-N}_b$ , then  $f_m$  is insensitive to background concentrations and these terms can be neglected (see Section 4 for further discussion of this assumption). In this case, Eqs. (3) and (4) reduce to

$$25 \quad Cl = f_m Cl_i, \quad (5)$$

$$\text{NO}_3\text{-N} = f_d (f_m \text{NO}_3\text{-N}_i). \quad (6)$$

Solving Eq. (6) for  $f_m$  and substituting into Eq. (5) yields

$$\frac{\text{NO}_3\text{-N}_i}{Cl_i} = \frac{1}{f_d} \frac{\text{NO}_3\text{-N}}{Cl}. \quad (7)$$

30 Thus, for each groundwater sample, the ratio of  $\text{NO}_3\text{-N}/\text{Cl}^-$  at the initial point of entry of the agriculturally derived  $\text{NO}_3^-$  to the groundwater system  $\left(\frac{\text{NO}_3\text{-N}_i}{Cl_i}\right)$  can be simply calculated using measured concentrations, and  $f_d$  estimated from  $\text{NO}_3^-$  isotope data. This provides a relatively simple method to identify agriculturally derived  $\text{NO}_3^-$  from different sources (e.g., EMS vs. manure piles) if they have different  $\text{NO}_3\text{-N}/\text{Cl}^-$  ratios. Estimated  $Cl_i$  and  $\text{NO}_3\text{-N}_i$  are reported as the mid-range value with uncertainty described by the minimum and maximum values. These initial concentrations are at the water table for top-down inputs, or at the saturated point of contact between the EMS and the aquifer for leakage from the EMS. This analysis assumes that a sampled water parcel consists of water with agriculturally derived  $\text{NO}_3^-$  that entered the aquifer from one source at one point in time and space and has since mixed with natural ambient groundwater. Any  $\text{NO}_3^-$  produced during nitrification after the anthropogenic

source water enters the aquifer is implicitly included in  $NO_3-N_i$ . The error in  $\frac{NO_3-N_i}{Cl_i^-}$  was assumed to be dominated by error in the estimated  $f_d$ , with the measurement error in  $NO_3-N$  and  $Cl^-$  considered negligible.

~~The amount of mixing is indicated by the fraction of source remaining ( $f_m$ ) and, therefore, the~~ The initial concentrations of the agriculturally derived  $NO_3^-$  source ( $NO_3-N_i$  and  $Cl_i^-$ ) were estimated by simultaneously solving Eqs. (5) and (6) using Excel Solver (GRG nonlinear). The absolute minimum values of  $NO_3-N_i$  and  $Cl_i^-$  were defined by measured concentrations (e.g., if  $Cl_i^- = Cl$ ,  $f_m = 1$ ). Maximum values of  $NO_3-N_i$  and  $Cl_i^-$  were defined based on measured concentrations of  $NO_3-N$  and  $Cl^-$  in groundwater and manure filtrate ( $NO_3-N \leq 150 \text{ mg L}^{-1}$  and  $Cl^- \leq 1300 \text{ mg L}^{-1}$ ; see Section 3.2). These maximum values of  $NO_3-N_i$  and  $Cl_i^-$  correspond to the minimum  $f_m$ . The value of  $f_d$  was assumed to be the mean  $f_d$  estimated from  $NO_3^-$  isotopes using Eq. (2), and  $\frac{NO_3-N_i}{Cl_i^-}$  was required to be within one standard deviation of the estimate from Eq. (7).

The resulting estimates of  $f_m$  are reported as the mid-range, with uncertainty described by the minimum and maximum values. Larger values of  $f_m$  indicate less mixing (a shorter path for advection-dispersion) and suggest a source close to the well. Smaller values of  $f_m$  indicate extensive mixing (a longer path for advection-dispersion) and suggest a source further away from the well. The relative contributions of mixing and denitrification to  $NO_3^-$  attenuation at each site were evaluated by comparing  $f_m$  and  $f_d$  for each sample. This analysis was conducted using isotope values from the samples collected on 1 May 2013 at CFO1, which were combined with the  $Cl^-$  and  $NO_3-N$  data from 6 June 2013. At CFO4, results from stable isotopes collected on 27 October 2014 were combined with  $Cl^-$  and  $NO_3-N$  data collected on 7 October 2014.

### 3. Results

#### 3.1 Site hydrogeology

##### 3.1.1 CFO1

The geology at CFO1 consists of clay and clay-till interspersed with sand layers of varying thickness to the maximum depth of investigation (20 m BG, bedrock not encountered). Hydraulic conductivities ( $K$ ) calculated from slug tests on wells ranged from  $1.2 \times 10^{-7}$  to  $4.2 \times 10^{-5} \text{ m-s}^{-1}$  ( $n=10$ ) for sand,  $1.1 \times 10^{-8}$  to  $2.8 \times 10^{-8} \text{ m s}^{-1}$  ( $n=2$ ) for clay-till, and  $1.6 \times 10^{-9}$  to  $3.0 \times 10^{-7} \text{ m s}^{-1}$  ( $n=8$ ) for clay. Depth to the water table throughout the study site ranged from 0.5 m at DMW14 to 3.8 m at DMW11. Seasonal water table variations were about 0.5 m with no obvious change in the annual average during the 6-year measurement period. Water table elevation was highest at DMW10 and DMW1 on the west side of the site and lowest at DMW11 on the northeast side of the site (see Supplementary Material). Measured heads indicate groundwater flow from the vicinity of the EMS to the northeast and southeast. Mean horizontal hydraulic gradients at the water table ranged from  $4.4 \times 10^{-3}$  to  $1.4 \times 10^{-2} \text{ m m}^{-1}$ . Vertical gradients were predominantly downward in the upper 20 m of the profile (mean gradients ranging from  $1.8 \times 10^{-3}$  to  $0.18 \text{ m m}^{-1}$ ), with the exception of DMW11 where the vertical gradient was upward (mean gradient  $-2.8 \times 10^{-2} \text{ m m}^{-1}$ ). Using the geometric mean  $K$  for the sand ( $5.0 \times 10^{-6} \text{ m s}^{-1}$ ) and a lateral head gradient of  $1.4 \times 10^{-2} \text{ m m}^{-1}$  yields a specific discharge (Darcy flux,  $q$ ) of  $2.2 \text{ m y}^{-1}$ . Assuming an effective porosity of 0.3 (Rodvang et al., 1998), the average linear velocity ( $\bar{v}$ ) is  $7.4 \text{ m y}^{-1}$ . This suggests that, in the absence of attenuation by mixing or denitrification, agriculturally derived  $NO_3^-$  could have been transported through the groundwater system by advection about 400 m from the EMS since 1960 and 630 m since 1930.

### 3.1.2 CFO4

The geology at CFO4 consists of about 5 m of clay (with minor till) underlain by sandstone, to the maximum depth investigated (20 m BG). Hydraulic conductivities measured using slug tests on wells were  $1.0 \times 10^{-8}$  to  $1.0 \times 10^{-5} \text{ m s}^{-1}$  ( $n=12$ ) for the clay and sandstone (many shallow wells were screened across the clay-till and into the sandstone) and  $1.0 \times 10^{-5}$  to  $2.9 \times 10^{-5} \text{ m s}^{-1}$  ( $n=4$ ) for the sandstone. The depth to water table ranged from 1.0 to 3.4 m, increasing from west to east across the study site. Seasonal water table variations were on the order of 1.5 m with water table declines on the order of  $0.3 \text{ m y}^{-1}$ . The horizontal hydraulic gradient was consistently from west to east, with a mean gradient at the water table of  $3.9 \times 10^{-3} \text{ m m}^{-1}$  between BC2 and BMW2 and  $4.3 \times 10^{-3} \text{ m m}^{-1}$  between BMW2 and BMW7. Vertical hydraulic gradients were  $4.2 \times 10^{-2}$  to  $4.6 \times 10^{-2} \text{ m m}^{-1}$  downward. Using the geometric mean  $K$  for the site ( $2.9 \times 10^{-5} \text{ m s}^{-1}$ ) and a lateral head gradient of  $4.3 \times 10^{-3} \text{ m m}^{-1}$  yields a  $q$  of  $0.4 \text{ m y}^{-1}$ . Assuming an effective porosity of 0.3 yields a  $\bar{v}$  of  $1.3 \text{ m y}^{-1}$ . These values suggest that, in the absence of attenuation by mixing or denitrification, anthropogenic  $\text{NO}_3^-$  could have been transported through the groundwater systems about 10 m by advection between 1995 and the time of sampling.

### 3.2 Values and evolution of stable isotopes of nitrate

Manure filtrate from the EMS at CFO1 had  $\delta^{15}\text{N}_{\text{NO}_3}$  ranging from 0.4 to 5.0‰ and  $\delta^{18}\text{O}_{\text{NO}_3}$  ranging from 7.1 to 19.0‰. ~~The evolution of  $\delta^{15}\text{N}_{\text{NO}_3}$  during nitrification can be modelled as a Rayleigh distillation process if the fraction factor is constant (Kendall and Aravena, 2000).~~ A curve showing the co-evolution of  $\delta^{18}\text{O}_{\text{NO}_3}$  (mixing of atmospheric  $\delta^{18}\text{O}$  with groundwater-derived  $\delta^{18}\text{O}$ ) and  $\delta^{15}\text{N}_{\text{NO}_3}$  (Rayleigh distillation,  $\beta = 1.005$ ) during nitrification is shown in Fig. 2. Isotopic values in DMW3, where direct leakage from the EMS was evident, are consistent with partial nitrification following this trend of isotopic evolution ( $\delta^{18}\text{O}_{\text{NO}_3}$  of -1.2‰ and  $\delta^{15}\text{N}_{\text{NO}_3}$  of 7.8‰).

The range of isotopic values of  $\text{NO}_3^-$  in groundwater is similar at both sites (Fig. 2). At CFO1,  $\delta^{18}\text{O}_{\text{NO}_3}$  ranged from -5.9 to 20.1‰ and  $\delta^{15}\text{N}_{\text{NO}_3}$  from -5.2 to 61.0‰. At CFO4,  $\delta^{18}\text{O}_{\text{NO}_3}$  ranged from -1.9 to 31.6‰ and  $\delta^{15}\text{N}_{\text{NO}_3}$  from -1.3 to 70.5‰. The isotopic values of  $\delta^{18}\text{O}_{\text{NO}_3}$  in groundwater are commonly assumed to be derived from a mix of a 1/3 atmospheric-derived oxygen (+23.5‰) and 2/3 water-derived oxygen (Xue et al., 2009). Given the average  $\delta^{18}\text{O}_{\text{H}_2\text{O}}$  for both sites (-16‰, see Supplementary Material), a 1/3 atmospheric 2/3 groundwater mix would result in a  $\delta^{18}\text{O}_{\text{NO}_3}$  of -3.7‰.

At both sites, co-enrichment of  $\delta^{18}\text{O}_{\text{NO}_3}$  and  $\delta^{15}\text{N}_{\text{NO}_3}$  characteristic of denitrification was evident in some samples (slopes of 0.42 and 0.72 in Fig. 2a). At CFO1, this includes samples from DP10-2, DMW5, DMW11, DMW12, DP11-12b, and DMW13 (and associated core) and some pore water from cores DC15-22 and DC15-23. These samples had  $\text{NO}_3\text{-N}$  concentrations of 0.6 to 23.7  $\text{mg L}^{-1}$ ,  $\delta^{18}\text{O}_{\text{NO}_3}$  ranging from 4.8 to 20.6‰, and  $\delta^{15}\text{N}_{\text{NO}_3}$  ranging from 22.9 to 61.3‰. At CFO4, samples exhibiting evidence of denitrification were from BMW2, BMW5, BMW6, BMW7, and BC4. These samples had  $\text{NO}_3\text{-N}$  concentrations ranging from 0.4 to 35.1  $\text{mg L}^{-1}$ ,  $\delta^{18}\text{O}_{\text{NO}_3}$  ranging from 1.6 to 22.1‰, and  $\delta^{15}\text{N}_{\text{NO}_3}$  ranging from 20.9 to 70.1‰. Although the isotopic values of DMW5 suggest enrichment by denitrification, the data plot away from the rest of the CFO1 data and close to the denitrification trend at CFO4 (Fig. 2), suggesting these samples were affected by some other process (possibly mixing or nitrification); therefore, the fraction of  $\text{NO}_3\text{-N}$  remaining in this well was not calculated. Also, well DMW3, which clearly receives leakage from the EMS, did not contain substantial  $\text{NO}_3\text{-N}$  and so  $f_d$  was not calculated.

The potential range of original isotopic values of the  $\text{NO}_3^-$  source prior to denitrification ( $R_0$ ) varied from 5 to 27‰ for  $\delta^{15}\text{N}_{\text{NO}_3}$  and from -2 to 7‰ for  $\delta^{18}\text{O}_{\text{NO}_3}$  based on isotopic values measured during this study (Fig. 2a). These values are consistent with literature values for manure-sourced  $\text{NO}_3^-$ , which report  $\delta^{15}\text{N}_{\text{NO}_3}$  ranging from 5 to 25‰ and  $\delta^{18}\text{O}_{\text{NO}_3}$  ranging from -5 to 5‰ (Wassenaar, 1995; Wassenaar et al., 2006; Singleton et al., 2007; McCallum et al., 2008; Baily et al., 2011).

The enrichment factor of  $\delta^{15}\text{N}_{\text{NO}_3}$  was defined by a normal distribution with a mean of -10‰ and standard deviation of 2.5‰. At CFO1, the coefficient of proportionality between the enrichment factor of  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  was described by a normal distribution with mean of 0.72 and standard deviation of 0.05. At CFO4, the coefficient of proportionality was also described by a normal distribution with a mean of 0.42 and standard deviation of 0.035 (see Fig. 2a). These enrichment factors are consistent with values from denitrification studies that report  $\epsilon_{15\text{N}}$  ranging from -4.0 to -30.0‰ and  $\epsilon_{18\text{O}}$  ranging from -1.9 to -8.9‰ (Vogel et al., 1981; Mariotti et al., 1988; Böttcher et al., 1990; Spalding and Parrott, 1994; Mengis et al., 1999; Pauwels et al., 2000; Otero et al., 2009).

### 3.3 Distribution and sources of agricultural nitrate in groundwater

At both sites TN concentrations in filtrate from the EMS and catch-basin were generally an order of magnitude larger than concentrations in groundwater (Table 2). The one exception is well DMW3 at CFO1 which intercepted direct leakage from the EMS (see 3.3.1 for further discussion of this well). In the EMS filtrate, N was predominately organic-N (TON up to 71%) or  $\text{NH}_3\text{-N}$  (up to 90%), with  $\text{NO}_x\text{-N}$  <0.1% of TN. In the catch-basin TON was >99% of TN. In groundwater TN concentrations ranged from <0.25 to 84.6 mg L<sup>-1</sup>, and this N was predominantly  $\text{NO}_3^-$  (again, with the exception of DMW3).

#### 3.3.1 CFO1

Agriculturally derived  $\text{NO}_3^-$  was predominantly restricted to the upper 20 m (or less) at CFO1 ( $\text{NO}_3\text{-N} \leq 0.2$  mg L<sup>-1</sup> and  $\text{Cl}^- \leq 57$  mg L<sup>-1</sup> in seven wells screened at 20 m). The one exception was DP11-12b, which had up to 4.1 mg L<sup>-1</sup> of  $\text{NO}_3\text{-N}$ . The southeast portion of the site also does not appear to have been significantly contaminated by agriculturally derived  $\text{NO}_3^-$ , with  $\text{NO}_3\text{-N}$  concentrations < 1 mg L<sup>-1</sup> in five water table wells (DMW4, DMW6, DMW14, DMW15, DMW16). In DMW6,  $\text{Cl}^-$  and ~~TN~~ concentrations were elevated (see Supplementary Material) but  $\text{NO}_3\text{-N}$  concentrations were < 2 mg L<sup>-1</sup>. Collectively, these data suggest the catch basin is not a significant source of  $\text{NO}_3^-$  to the groundwater at this site.

Leakage of manure slurry from the EMS at CFO1 is clearly indicated by the data from DMW3, which feature the highest concentrations of TN in groundwater (up to 548 mg L<sup>-1</sup>) and elevated  $\text{Cl}^-$ ,  $\text{HCO}_3^-$ , and DOC in concentrations similar to EMS manure filtrate (see Supplementary Material). Nevertheless,  $\text{NO}_3\text{-N}$  concentrations in this well were consistently low ( $1.1 \pm 2.7$  mg L<sup>-1</sup>, n=22). The potential for nitrification in the vicinity of this well is indicated by  $\text{NO}_2\text{-N}$  production ( $2.7 \pm 8.3$  mg L<sup>-1</sup>, n=22). However, the data demonstrate that only a small proportion of the  $\text{NH}_3\text{-N}$  in DMW3 ( $373.4 \pm 79.4$  mg L<sup>-1</sup>, n=22) could have been converted to  $\text{NO}_3^-$  within the subsurface ( $\text{NO}_3\text{-N}$  in groundwater  $\leq 66$  mg L<sup>-1</sup>) ( $\text{NO}_3\text{-N}/\text{Cl}^-$  ratio of 0.95).

The maximum  $\text{NO}_3\text{-N}$  concentration in groundwater was measured in core sample DC15-23 (clay at 2 m bgl, 7 m hydraulically downgradient of DMW3). The  $\text{NO}_3\text{-N}$  in this core sample was most likely introduced into the groundwater system by vertical infiltration or diffusion from above. Pore water extracted from the unsaturated

zone (sand) at the top of this core profile contained 865 mg L<sup>-1</sup> of NO<sub>3</sub>-N and had a NO<sub>3</sub>-N/Cl<sup>-</sup> ratio of 1.04, consistent with the ratio of 0.95 in the core sample.

Contamination by agricultural NO<sub>3</sub><sup>-</sup> that exceeds the drinking water guidelines (NO<sub>3</sub>-N > 10 mg L<sup>-1</sup>) was observed in wells up to 40 m hydraulically downgradient of the EMS (DMW13, DP10-2) and in well DMW11 situated 470  
5 from the EMS (Fig. 3). DMW1, located upgradient of the EMS, also had concentrations of NO<sub>3</sub>-N > 10 mg L<sup>-1</sup> with an increasing trend, but the source of this NO<sub>3</sub><sup>-</sup> is not clear. DMW2 and DMW12 also had NO<sub>3</sub>-N concentrations that were elevated but did not exceed the drinking water guideline (≤ 3.7 mg L<sup>-1</sup>).

Given the evidence of incomplete partial nitrification in DMW3, the NO<sub>3</sub>-N/Cl<sup>-</sup> ratio of contamination from the EMS was assumed to be best represented by DP10-2, which is located directly downgradient of the EMS. Data  
10 for this well indicate values of NO<sub>3</sub>-N/Cl<sup>-</sup> predominantly ranging from 0.1 to 0.3 with  $NO_3-N_i/Cl_i$  estimated at  $0.3 \pm 0.13$  (Fig. 4). Advective transport from DMW3 is also the likely source of NO<sub>3</sub>-N (up to 21.1 mg L<sup>-1</sup>) within the sand between 6 and 12 m depth in DC15-23. NO<sub>3</sub>-N/Cl<sup>-</sup> ratios in these samples ranged from 0.07 to 0.31, consistent with DP10-2. Stable isotope values in pore water from this sand layer do not indicate substantial denitrification ( $\delta^{18}O \leq 5.9\%$ ,  $\delta^{15}N \leq 16.7\%$ ), suggesting these ratios will be similar to the initial ratios at the point  
15 of entry to the groundwater system.

In contrast, the ratio of  $NO_3-N_i/Cl_i$  in DMW13 (33 m downgradient from DP10-2) was  $0.75 \pm 0.29$ , which is more similar to the NO<sub>3</sub>-N/Cl<sup>-</sup> ratio in DC15-23 at 2 m (0.95), which is interpreted as reflecting a top-down source. The NO<sub>3</sub><sup>-</sup> in DMW13 is therefore unlikely to be sourced solely from leakage from the EMS, and could be sourced from the adjacent dairy pens or a temporary manure pile that was observed adjacent to this well during core  
20 collection in 2015 (or a combination of EMS and top-down sources).

The  $NO_3-N_i/Cl_i$  ratio in DMW12 is not inconsistent with an EMS source, but the hydraulic gradient between DMW2 and DMW12 is negligible, indicating a lack of driving force for advective transport from the EMS towards DMW12. This is also the case for well DMW1, which is upgradient of the EMS but had elevated NO<sub>3</sub>-N concentrations ( $6.5 \pm 3.6$ , n=18). The source of nitrate in these wells is therefore unlikely to be related to leakage  
25 from the EMS, but alternative sources (i.e., nearby temporary manure piles) are not known.

Well DMW11 had consistently low NO<sub>3</sub>-N/Cl<sup>-</sup> ratios (< 0.05). The  $NO_3-N_i/Cl_i$  ratio indicated by DMW11 was similar to DP10-2, but estimates of  $Cl_i$  indicate Cl<sup>-</sup> sourced from inputs with three-fold higher Cl<sup>-</sup> concentrations than the source to DP10-2 (Fig. 4b). Well DMW11 is located hydraulically downgradient of feedlot pens and adjacent to a solid manure storage area. Well DMW11 is also in a local topographic low and is likely receiving  
30 NO<sub>3</sub>-N and Cl<sup>-</sup> from surface runoff and infiltration in addition to subsurface groundwater flow. Well DMW11 had high  $NO_3-N_i$  and  $Cl_i$  consistent with measured values in that well, indicating a local top-down source that is likely the nearby solid manure pile.

### 3.3.2 CFO4

At CFO4, measured data indicate that effects from agricultural operations on NO<sub>3</sub><sup>-</sup> concentrations in groundwater are restricted to the upper 15 m of the subsurface. NO<sub>3</sub>-N concentrations in wells screened at 15 m depth were  
35 < 0.5 mg L<sup>-1</sup>, with the exception of one sample from BP10-15w (May 2012) with 4.3 mg L<sup>-1</sup> of NO<sub>3</sub>-N. Water table wells in the west and north of the study site (BC1, BC2, and BC3) also indicate negligible impacts of agricultural operations, with Cl<sup>-</sup> < 10 mg L<sup>-1</sup> and NO<sub>3</sub>-N < 0.1 mg L<sup>-1</sup>.

Concentrations of  $\text{NO}_3\text{-N} > 10 \text{ mg L}^{-1}$  were measured in three water table wells (BMW2, BMW3, BMW4) installed adjacent to the EMS (Fig. 5). Of these, BMW2 had much higher  $\text{Cl}^-$  concentrations ( $502 \pm 97 \text{ mg L}^{-1}$ ,  $n=22$ ), and therefore lower  $\text{NO}_3\text{-N}/\text{Cl}^-$  ratios ( $< 0.05$ ). Given the elevated  $\text{Cl}^-$  concentrations in this well were consistent with concentrations in the EMS, direct leakage from the EMS was assumed to be the source. Stable isotopes of  $\text{NO}_3^-$  indicate substantial denitrification in BMW2, with estimated  $\text{NO}_3\text{-N}_i \geq 127 \text{ mg L}^{-1}$  and an  $\text{NO}_3\text{-N}_i/\text{Cl}_i$  ratio of 0.1 to 0.3 (Fig. 6). This ratio is consistent with data from well BMW4, which is immediately adjacent to the EMS (on the upgradient side) and likely reflects leakage from the EMS without denitrification (based on stable isotopes of  $\text{NO}_3^-$ ).  $\text{NO}_3\text{-N}/\text{Cl}^-$  ratios measured in BMW4 were predominantly 0.1 to 0.3, consistent with the reconstructed  $\text{NO}_3\text{-N}_i/\text{Cl}_i$  ratio in BMW2.

Agriculturally derived  $\text{NO}_3^-$  in other wells not immediately adjacent to the EMS is unlikely to be related to leakage from the EMS. Wells BMW5 and BMW7 are 60 and 140 m hydraulically downgradient from the EMS, respectively.  $\text{NO}_3\text{-N}_i/\text{Cl}_i$  ratios in these wells were not inconsistent with BMW2 (i.e., the range of values overlap), but advective transport is only likely to have transported solutes around 10 m since the EMS was installed (see Section 3.1.2). As such, the source of  $\text{NO}_3\text{-N}$  in these wells is likely the dairy pens rather than the EMS.

Concentrations of  $\text{NO}_3\text{-N} > 10 \text{ mg L}^{-1}$  were also measured in BC4, which is located 95 m hydraulically upgradient of the EMS. The ratio of  $\text{NO}_3\text{-N}_i/\text{Cl}_i$  at BC4 was the highest at CFO4 (0.6) and did not overlap with BMW2. This indicates that the  $\text{NO}_3^-$  in this well was sourced from an adjacent manure pile, which was observed during the study.

### 3.4 Mechanisms of attenuation of agriculturally derived $\text{NO}_3^-$

Attenuation of agriculturally derived  $\text{NO}_3^-$  in groundwater is dominated by denitrification at CFO1 and CFO4, with estimates of  $f_m$  consistently higher than estimates of  $f_d$  (Table 23, Fig. 7, Table S10). Calculated  $f_d$  values suggest that at least half of the  $\text{NO}_3\text{-N}$  present at the initial point of entry to the groundwater system has been removed by denitrification. ~~The substantial uncertainty in  $f_m$  is related to the range of  $\text{NO}_3\text{-N}_i$  and  $\text{Cl}_i$ , with the largest uncertainty corresponding to the lowest measured concentrations (i.e., furthest from the upper limit).~~ Comparison of  $\text{NO}_3\text{-N}_{\text{mix}}$  (the concentration of  $\text{NO}_3\text{-N}$  that would be measured if mixing was the only attenuation mechanism) with measured concentrations (which reflect attenuation by both mixing and denitrification) suggests that the sample from 20 m depth (DP11-12b) is the only sample that would be below the drinking water guideline if mixing was the only attenuation mechanism (Fig. 8).

At both sites, the stable isotope values of  $\text{NO}_3^-$  indicate that denitrification proceeds within metres of the source.

At CFO1, calculated  $f_d$  in well DP10-2 (2 m from the EMS) is  $0.52 \pm 0.22$ ; at CFO4,  $f_d$  in well BMW2 (3 m from the EMS) is  $0.13 \pm 0.06$ . Denitrification also substantially attenuated  $\text{NO}_3\text{-N}$  concentrations in wells where the source is not the EMS but instead is adjacent solid manure piles (e.g., DMW11 at CFO1, BC4 at CFO4). In BMW6 at CFO4, denitrification completely attenuated the agriculturally derived  $\text{NO}_3^-$ . This well had negligible  $\text{NO}_3\text{-N}$  ( $0.4 \pm 0.2 \text{ mg L}^{-1}$ ,  $n=8$ ) and the lowest  $f_d$  of 0.01. Measured DOC in this well was consistent with other wells at both sites ( $6.9 \pm 1.7 \text{ mg L}^{-1}$ ,  $n=3$ ), suggesting DOC depletion does not limit denitrification at these CFO operations. Calculated  $f_d$  and  $f_m$  should decrease with increasing subsurface residence time and distance from source. Data from wells support the source identification based on concentrations of  $\text{NO}_3\text{-N}$  and  $\text{Cl}^-$  and  $\text{NO}_3\text{-N}/\text{Cl}^-$  ratios (see Section 3.3). Well DMW11 (470 m from the EMS) had the highest  $f_m$  at CFO1 (0.83), indicating less mixing and suggesting the anthropogenic source of  $\text{NO}_3^-$  in this well is relatively close, which is consistent with the adjacent

the solid manure pile being the source of  $\text{NO}_3^-$  to this well. At CFO4, well BMW2, which is adjacent to the EMS, had the highest  $f_m$  (0.92), indicating the least attenuation of  $\text{NO}_3^-$  by mixing and consistent with the EMS being the source of  $\text{NO}_3^-$  to this well.

#### 5 4. Discussion

Agriculturally derived  $\text{NO}_3^-$  at these two sites with varying lithology is generally restricted to depths  $< 20$  m, consistent with previous studies at CFOs (Robertson et al., 1996; Rodvang and Simpkins, 2001; Rodvang et al., 2004; Kohn et al., 2016). Attenuation of agriculturally derived  $\text{NO}_3^-$  in groundwater is a spatially varying combination of mixing and denitrification, with denitrification playing a greater role than mixing at both sites. In the samples for which  $f_d$  could be determined, denitrification reduced  $\text{NO}_3^-$  concentrations by at least half and, in some cases, back to background concentrations. Given that the range of source isotopic composition was allowed to vary to its maximum justifiable extent, these quantitative estimates of denitrification based on stable isotopes of  $\text{NO}_3^-$  are likely to be conservative. Denitrification appears to proceed within metres of the  $\text{NO}_3^-$  source, suggesting relatively short residence times and redox conditions at the water table may be conducive to denitrification reactions (Critchley et al., 2014; Clague et al., 2015). ~~The combination of the approach outlined here with measurement of groundwater age indicators would allow for better constraints on groundwater flow velocities and determination of denitrification rates (Böhlke and Denver, 1995; Katz et al., 2004; McMahon et al., 2004; Clague et al., 2015).~~

The substantial role of denitrification within the saturated glacial sediments at these study sites indicates the potential for significant attenuation of agriculturally derived  $\text{NO}_3^-$  by denitrification in similar groundwater systems across the North American interior and Europe (Ernstsen et al., 2015; Zirkle et al., 2016). Denitrification in the unsaturated zone is limited by low water contents and oxic conditions, resulting in substantial stores of  $\text{NO}_3^-$  in vadose zones (Turkeltaub et al., 2016; Ascott et al., 2017).  $\text{NO}_3^-$  in water that is removed rapidly from site is also unlikely to be substantially attenuated by denitrification due to oxic conditions and rapid transit times (Ernstsen et al., 2015). Therefore, water management focussed on reducing the effects of  $\text{NO}_3^-$  contamination in similar hydrogeological settings to this study should aim to maximize infiltration into the saturated zone where  $\text{NO}_3^-$  concentrations can be naturally attenuated, provided that local groundwater isn't used for potable water supply.

Infiltration of  $\text{NO}_3^-$  rich water that has passed through temporary solid manure piles and dairy pens has resulted in groundwater  $\text{NO}_3^-$ -N concentrations as high as those associated with leakage from the EMS (e.g., DMW11, DMW13, BC4). At CFO4, this is in spite of the presence of clay at surface, which is attributable to secondary porosity in the upper part of the profile that has led to hydraulic conductivities comparable to sand. This ~~result~~ is consistent with the findings of Showers et al. (2008), who investigated sources of  $\text{NO}_3^-$  at an urbanized dairy farm in North Carolina, USA. The limited impact of construction of EMS facilities in Alberta has been regulated under the Agriculture Operation Practices Act since 2002, which requires them to be lined with clay to minimise leakage (Lorenz et al., 2014). The results of this study suggest that on-farm waste management should increasingly focus on minimising temporary manure piles that are in direct contact with the soil to reduce  $\text{NO}_3^-$  contamination associated with dairy farms and feedlots.

~~The absence of direct leakage from the EMS on  $\text{NO}_3^-$  concentrations in groundwater at these sites may be partly due to the relatively shallow water table and CFO4~~ suggests that saturation within the clay lining of the EMS ~~may have~~has limited the development of extensive secondary porosity that would allow rapid water percolation (Baram et al., 2012). Elevated  $\text{NH}_3\text{-N}$  concentrations in the water table well at the southeast corner of the EMS at CFO1 (DMW3) ~~do~~ indicate direct leakage from the EMS, but because nitrification within the EMS is minimal, this has not resulted in elevated  $\text{NO}_3\text{-N}$  in this well. Two possibilities for the fate of  $\text{NH}_3\text{-N}$  in DMW3 are attenuation by cation exchange and oxidation to  $\text{NO}_3\text{-N}$  within the groundwater system. Measured  $\text{NO}_3\text{-N}$  concentrations in groundwater represent only a small fraction ( $\leq 10\%$ ) of  $\text{NH}_3\text{-N}$  within the EMS (or DMW3), suggesting oxidation to  $\text{NO}_3^-$  within the aquifer may be limited. Further work is required to assess the importance of cation exchange as an attenuation mechanism for direct leakage from the EMS at this site.

The sources of manure-derived  $\text{NO}_3^-$  (manure piles vs. EMS) are distinguishable based on  $\text{NO}_3\text{-N}_i/\text{Cl}_i$  ratios, provided there is also an understanding of the history of each site, local hydrogeology, and potential sources. Estimation of  $\text{NO}_3\text{-N}_i/\text{Cl}_i$  assumes that background concentrations could be neglected in the mixing calculation. The error associated with this assumption increases as source concentrations and measured concentrations approach background concentrations. At these study sites, background concentrations are likely to be  $< 20 \text{ mg L}^{-1}$  for  $\text{Cl}^-$  and  $< 1 \text{ mg L}^{-1}$  for  $\text{NO}_3\text{-N}$ . Based on these values, estimated  $\text{NO}_3\text{-N}_i$  values are at least 20 times background  $\text{NO}_3\text{-N}$  concentrations, and over 100 times background concentrations in some wells. The estimated  $\text{Cl}_i$  values are at least three times background concentrations at CFO1 and at least 10 times background concentrations at CFO4.

~~Measured~~In this study we applied a two-end member mixing model and assumed that background concentrations can be neglected. The error introduced by neglecting background concentrations was assessed by comparing  $f_m$  calculated with and without background concentrations included, using the full range of values in this study (Fig. 9). ~~Neglecting background concentrations results in overestimation of  $f_m$  (i.e. underestimation of the amount of attenuation mixing) with the largest errors when measured concentrations are closer~~close to background concentrations ~~than initial concentrations, but neglecting background concentrations~~. For  $\text{Cl}^-$  the maximum difference of 0.13 is still likely to be a small source of error relative ~~the~~in the mid-range of  $f_m$  values. For  $\text{NO}_3\text{-N}$ , the difference is consistently  $< 0.1$  with the largest errors at the lowest values of  $f_m$ . The uncertainty in ~~maximum~~ concentrations. For example, well DMW13 had the lowest measured  $\text{Cl}^-$  concentration ( $57 \text{ mg L}^{-1}$ ); if we assume a  $\text{Cl}_b$  of  $10 \text{ mg L}^{-1}$  and a  $\text{Cl}_i$  of  $100 \text{ mg L}^{-1}$ , the error in  $f_m$  introduced by neglecting  $\text{Cl}_b$  is 9%; if  $\text{Cl}_b/f_m$  is  $20 \text{ mg L}^{-1}$ , the error is 23%. The accuracy of  $\text{NO}_3\text{-N}_i/\text{Cl}_i$  is determined by the accuracy of  $f_d$ , and the primarily related to uncertainty ~~is independent of the measured concentrations of  $\text{NO}_3^-$  and  $\text{Cl}^-$~~ . Uncertainty in the initial concentrations ( $\text{Cl}_i$  and  $\text{NO}_3\text{-N}_i$ ), which depends on measured  $\text{Cl}^-$  and  $\text{NO}_3\text{-N}$ . The largest uncertainties in  $\text{NO}_3\text{-N}_i$  and  $\text{Cl}_i$  correspond to the lowest measured concentrations (i.e., furthest from the upper limit), with less uncertainty at higher measured concentrations as they approach the maximum values. Temporal variability in  $\text{NO}_3\text{-N}_i/\text{Cl}_i$  for each source could not be determined based on the snapshot isotope sampling conducted, but this could be investigated by measuring  $\text{NO}_3^-$  isotopes in conjunction with  $\text{NO}_3\text{-N}$  and  $\text{Cl}^-$  at multiple times.

~~Although applicable at these sites, this approach may not be valid at other sites if additional sources of  $\text{NO}_3^-$  in groundwater (e.g. fertilizer or nitrification) are significant, or if  $\text{NO}_3^-$  concentrations in groundwater are naturally elevated (Hendry et al., 1984). The combination of the approach outlined here with measurement of groundwater age indicators would allow for better constraints on groundwater flow velocities and determination of denitrification rates (Böhlke and Denver, 1995; Katz et al., 2004; McMahon et al., 2004; Clague et al., 2015).~~

Nitrate isotope values in groundwater at the two CFOs studied are generally consistent with previous studies reporting denitrification of manure-derived  $\text{NO}_3^-$  at dairy farms (Wassenaar, 1995; Wassenaar et al., 2006; Singleton et al., 2007; McCallum et al., 2008; Baily et al., 2011). However, a number of groundwater samples collected for the present study had relatively enriched  $\delta^{18}\text{O}_{\text{NO}_3}$  ( $> 15\text{‰}$ ) with depleted  $\delta^{15}\text{N}_{\text{NO}_3}$  ( $< 15\text{‰}$ ). Some of these isotopic values are within the range previously reported for  $\text{NO}_3^-$  derived from inorganic fertilizer ( $\delta^{15}\text{N}_{\text{NO}_3}$  from  $-3$  to  $3\text{‰}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  from  $-5$  to  $25\text{‰}$ ), with the  $\delta^{18}\text{O}_{\text{NO}_3}$  depending on whether the  $\text{NO}_3^-$  is from  $\text{NH}_4^+$  or  $\text{NO}_3^-$  in the fertilizer (Mengis et al., 2001; Wassenaar et al., 2006; Xue et al., 2009). To the best of our knowledge, however, no inorganic fertilizers have been applied at these study sites. Another potential source is  $\text{NO}_3^-$  derived from soil organic N, but this should have  $\delta^{15}\text{N}_{\text{NO}_3}$  values of  $0$  to  $10\text{‰}$  and  $\delta^{18}\text{O}_{\text{NO}_3}$  values of  $-10$  to  $15\text{‰}$  (Durka et al., 1994; Mayer et al., 2001; Mengis et al., 2001; Xue et al., 2009; Baily et al., 2011). Incomplete nitrification of  $\text{NH}_4^+$  can result in  $\delta^{15}\text{N}_{\text{NO}_3}$  lower than the manure source (Choi et al., 2003), but as there was no measurable  $\text{NH}_3\text{-N}$  in these samples this is also unlikely. These isotope values may reflect the influence of  $\text{NO}_3^-$  from precipitation, which usually has values ranging from  $-5$  to  $5\text{‰}$  for  $\delta^{15}\text{N}_{\text{NO}_3}$  and  $40$  to  $60\text{‰}$  for  $\delta^{18}\text{O}_{\text{NO}_3}$ , and has been reported to dominate  $\text{NO}_3^-$  isotope values of groundwater under forested landscapes (Durka et al., 1994). Alternatively, they may be affected by microbial immobilization and subsequent mineralization and nitrification, which can mask the source  $\delta^{18}\text{O}_{\text{NO}_3}$  in aquifers with long residence times (Mengis et al., 2001; Rivett et al., 2008). The isotopic values of  $\text{NO}_3^-$  in the manure filtrate from the EMS at CFO1, were generally inconsistent with values for manure-sourced  $\text{NO}_3^-$  reported in other groundwater studies (Wassenaar, 1995; Wassenaar et al., 2006; Singleton et al., 2007; McCallum et al., 2008a; Baily et al., 2011). This is likely to be because nitrification within the EMS was negligible ( $\text{NO}_3\text{-N} < 0.7 \text{ mg L}^{-1}$ ), such that the isotopic values of  $\text{NO}_3\text{-N}$  in the manure filtrate reflect volatilization of  $\text{NH}_3$  and partial nitrification within the EMS.  $\delta^{18}\text{O}_{\text{NO}_3}$  values may also have been affected by evaporative enrichment of the  $\delta^{18}\text{O}_{\text{H}_2\text{O}}$  being incorporated into  $\text{NO}_3^-$  (Showers et al., 2008).

## 5. Conclusions

~~Quantitative~~ A mixing model constrained by quantitative estimates of denitrification ~~based on the stable isotopic value of  $\text{NO}_3^-$  in groundwater were used to constrain a binary mixing model based on  $\text{Cl}^-$  and  $\text{NO}_3\text{-N}$  from isotopes~~ substantially improved our understanding of nitrate contamination at these sites. This novel approach ~~allowed the identification~~ has the potential to be widely applied as a tool for monitoring and assessment of  $\text{NO}_3\text{-N}$  sources and quantification of mixing and denitrification as mechanisms of  $\text{NO}_3^-$  attenuation in groundwater at two dairy farms overlying groundwater in complex agricultural settings. Even though these sites are dominated by clay-rich glacial sediments, ~~Relative to leakage from the EMS,~~ the input of  $\text{NO}_3^-$  to groundwater from temporary manure piles and pens resulted in comparable (or greater)  $\text{NO}_3\text{-N}$  concentrations ~~in groundwater at these sites than leakage from the EMS. On-farm management of manure waste should increasingly focus on limiting manure piles that are in direct contact with the soil to limit  $\text{NO}_3^-$  contamination of groundwater.~~ Nitrate attenuation at both sites is dominated by denitrification, which is evident even in wells directly adjacent to the  $\text{NO}_3^-$  source. On-site denitrification reduced agriculturally derived  $\text{NO}_3^-$  concentrations by at least half and, in some wells, completely. These results indicate that infiltration to groundwater systems in glacial sediments where  $\text{NO}_3^-$  can be naturally attenuated is likely to be preferable to off-farm export via runoff or drainage networks, provided that local groundwater isn't a potable water source.

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**Table 1. Details of groundwater monitoring wells and continuous core collection at CFO1 and CFO4 (all screens installed at bottom of the well).**

Site	Well/Core hole ID	Type <sup>†</sup>	Lateral distance from EMS* (m)	Ground elevation (m asl)	Total depth (m below ground)	Screen length (m)	Lithology of screened interval	K (m s <sup>-1</sup> )
CFO1	DMW1	WTW	60	869.7	5.0	4.0	Sand	
	DMW2	WTW	10	867.2	6.0	4.0	Sand	1.2 × 10 <sup>-7</sup>
	DMW3	WTW	2	867.5	3.7	2.0	Sand	
	DMW4	WTW	160		4.2	4	Sand	1.3 × 10 <sup>-6</sup>
	DMW5	WTW	270	866.4	6.8	4.0	Clayey sand	1.7 × 10 <sup>-5</sup>
	DMW6	WTW	310		6.7	4		
	DP10-1	Piezo	2	867.8	18.6	0.5	Clay	1.6 × 10 <sup>-9</sup>
	DP10-2	Piezo	2	867.9	8.0	1.5	Sand	3.6 × 10 <sup>-5</sup>
	DMW10	WTW	340	868.0	7.2	3.0	Clay	3.0 × 10 <sup>-7</sup>
	DP11-10b	Piezo	340	868.0	20	0.5	Clay	2.2 × 10 <sup>-8</sup>
	DMW11	WTW	470	864.8	7.0	3.0	Sand and clay	4.2 × 10 <sup>-5</sup>
	DP11-11b	Piezo	470		20	0.5	Clay	6.3 × 10 <sup>-9</sup>
	DMW12	WTW	50	867.6	7.0	3.0	Sand and clay	7.4 × 10 <sup>-6</sup>
	DP11-12b	Piezo	50	867.6	20.1	1.0	Clay	1.1 × 10 <sup>-8</sup>
	DMW13	WTW	35	867.1	7.0	3.0	Sand	8.9 × 10 <sup>-6</sup>
	DP11-13b	Piezo + core	35	867.1	20.0	0.5	Clay	
	DMW14	WTW	105	865.7	7.0	3.0	Clay	5.7 × 10 <sup>-6</sup>
	DP11-14b	Piezo	105	865.7	20.0	0.5	Sand	1.1 × 10 <sup>-6</sup>
	DMW15	WTW	185		7.0	3	Clay	2.4 × 10 <sup>-8</sup>
	DP11-15b	Piezo	185		20.0	0.5	Clay	1.4 × 10 <sup>-7</sup>
	DMW16	WTW	320	866.0	6.0	3.0	Sand and clay	-
	DP11-16b	Piezo	320		20.0	0.5	Clay	3.2 × 10 <sup>-9</sup>
	DC15-20	Core	76		15			
DC15-21	Core	45		10.5				
DC15-22	Core	22		12				
DC15-23	Core	9		15				
CFO4	BC1	WTW	110	857.0	6.9	3.1	Clay and sandstone	
	BC2	WTW	365	859.4	7.0	3.1	Clay and sandstone	2.2 × 10 <sup>-7</sup>
	BC3	WTW	145	858.6	6.8	3.1	Clay and sandstone	1.3 × 10 <sup>-6</sup>
	BC4	WTW	95	858.8	5.9	3.0	Clay and sandstone	3.4 × 10 <sup>-6</sup>
	BC5	WTW	105	859.5	7.5	4.5	Clay and sandstone	
	BMW1	WTW	4	858.6	7.1	3.1	Clay and sandstone	4.3 × 10 <sup>-6</sup>
	BMW2	WTW	3	857.9	7.5	4.5	Clay and sandstone	8.5 × 10 <sup>-7</sup>
	BMW3	WTW	8	858.6	6.0	3.0	Clay and sandstone	
	BMW4	WTW	14	858.0	7.5	4.8	Clay and sandstone	1.0 × 10 <sup>-5</sup>
	BMW5	WTW	60	858.0	7.5	4.5	Clay and sandstone	
	BP5-15	Piezo	60	858.1	15.3	1.5	Sandstone	1.0 × 10 <sup>-7</sup>
	BMW6	WTW	150	856.9	7.5	4.5	Clay and sandstone	4.0 × 10 <sup>-6</sup>
	BP6-15	Piezo	150	856.8	15.2	1.5	Sandstone	3.0 × 10 <sup>-6</sup>
	BMW7	WTW	140	856.7	7.5	4.5	Clay and sandstone	1.0 × 10 <sup>-6</sup>
	BP10-15e	Piezo	4	858.2	14.9	1.5	Sandstone	2.9 × 10 <sup>-5</sup>
BP10-15w	Piezo	10	858.0	15.0	1.5	Sandstone	1.0 × 10 <sup>-5</sup>	

\*EMS=Earthen manure storage

<sup>†</sup>WTW=water table well, Piezo = piezometer, Core = continuous core

**Table 2. Measured Cl<sup>-</sup> and NO<sub>3</sub><sup>-</sup> concentrations and stable isotopic values of NO<sub>3</sub><sup>-</sup> and estimated  $f_a$ ,  $f_m$ . Range of measured concentrations of TN, NH<sub>3</sub>-N, NO<sub>x</sub>-N (NO<sub>2</sub>-N + NO<sub>3</sub>-N) and TON at each study site. At CFO1 results from monitoring well DMW3 are presented separately because values in this well differed substantially from all other wells.**

Site	N-pool	TN (mg L <sup>-1</sup> )	NH <sub>3</sub> -N (mg L <sup>-1</sup> )	NO <sub>x</sub> -N (mg L <sup>-1</sup> )	TON (mg L <sup>-1</sup> )
CFO1	EMS	550 – 1820	275 – 747	<0.1 – 0.4	73 – 1301
	Catch-basin	200 – 1440	2.5 – 7.3	<0.1	196 – 1437
	DMW3	278 – 548	219 – 479	<0.1 – 50 <sup>*</sup>	31.3 – 73.9
	Other monitoring wells	<0.25 – 33.4	<0.05 – 2.9	<0.1 – 31.4 <sup>**</sup>	<0.2 – 3.7
CFO4	EMS <sup>†</sup>	1000 – 1240	724 – 747	0.25 – 0.29	275 – 492
	Monitoring wells	<0.25 – 84.6	<0.05 – 0.23	<0.1 – 80.4	<0.2 – 13.9

<sup>\*</sup>NO<sub>x</sub>-N of 50 mg L<sup>-1</sup> in DMW3 consisted of 12.6 mg L<sup>-1</sup> as NO<sub>3</sub>-N and 37.4 mg L<sup>-1</sup> as NO<sub>2</sub>-N.

<sup>\*\*</sup>NO<sub>x</sub>-N max in groundwater measured in core (NO<sub>3</sub>-N = 66.4 mg L<sup>-1</sup>, NO<sub>2</sub>-N = 67.8 mg L<sup>-1</sup>)

<sup>†</sup>Range across three replicates measured on 25 August 2011

**Table 3. Calculated  $f_a$  and  $f_m$  based on measured Cl<sup>-</sup> and NO<sub>3</sub>-N concentrations and stable isotope values of NO<sub>3</sub><sup>-</sup>.**

Study area	Sample ID*	Cl <sup>-</sup> (mg L <sup>-1</sup> )	NO <sub>3</sub> -N (mg L <sup>-1</sup> )	δ <sup>15</sup> N <sub>NO3</sub> (‰)	δ <sup>18</sup> O <sub>NO3</sub> (‰)	$f_a$ (mean ± stdev)	$f_m$ <sup>**</sup> (mid-range)
CFO1	DP11-13_4.3m	28.5	7.0	30.3	9.8	0.30 ± 0.15	0.58
	DP11-13_5.2m	25.0	7.8	31.0	10.8	0.34 ± 0.13	0.58
	DP11-13_7m	72.3	12.0	31.6	10.2	0.27 ± 0.13	0.65
	DP11-13_7.9m	70.8	9.1	36.4	14.0	0.17 ± 0.09	0.68
	DP11-13_8.8m	81.7	10.9	29.6	9.9	0.32 ± 0.15	0.63
	DC15-22_6.5m	99.2	4.7	30.8	16.8	0.19 ± 0.08	0.58
	DC15-22_10m	73.0	11.0	26.1	7.4	0.47 ± 0.21	0.63
	DP10-2	74.5	11.8	24.2	4.8	0.52 ± 0.22	0.63
	DMW11	436.1	17.1	33.3	10.9	0.17 ± 0.07	0.83
	DMW12	78.0	2.57	29.8	14.3	0.23 ± 0.10	0.54
	DMW13	56.7	23.7	23.0	6.8	0.56 ± 0.22	0.65
	DP11-12b	95.7	0.6	35.9	17.0	0.15 ± 0.08	0.54
CFO4	BC4	163.1	35.1	30.6	1.6	0.37 ± 0.13	0.82
	BMW2	595.6	16.5	41.6	8.3	0.13 ± 0.06	0.92
	BMW5	131.2	12.9	28.9	6.5	0.34 ± 0.16	0.63
	BMW6	156.0	0.4	70.5	22.1	0.01 ± 0.01	0.56
	BMW7	134.7	11.6	34.0	5.9	0.21 ± 0.11	0.68

\*central depth of core samples, x, indicated as SampleID\_xm.

\*\* maximum  $f_m$  is 1 for all samples, which implies no mixing.

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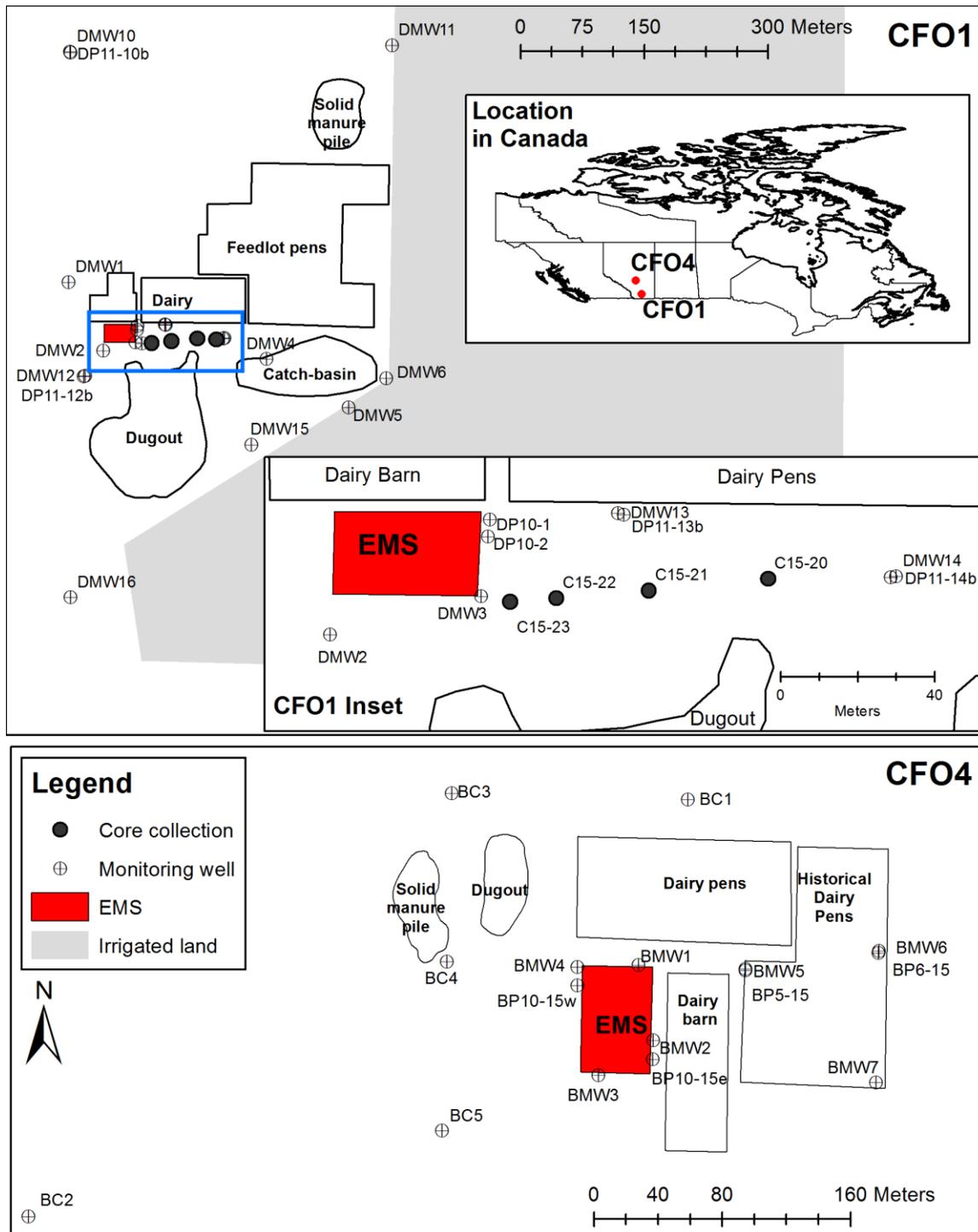


Figure 1: Map of study sites CFO1 and CFO4, showing locations of groundwater monitoring wells, core collection, earthen manure storages (EMS), dairy and feedlot pens, manure piles, and irrigated land. Blue rectangle indicates extent of CFO1 inset.

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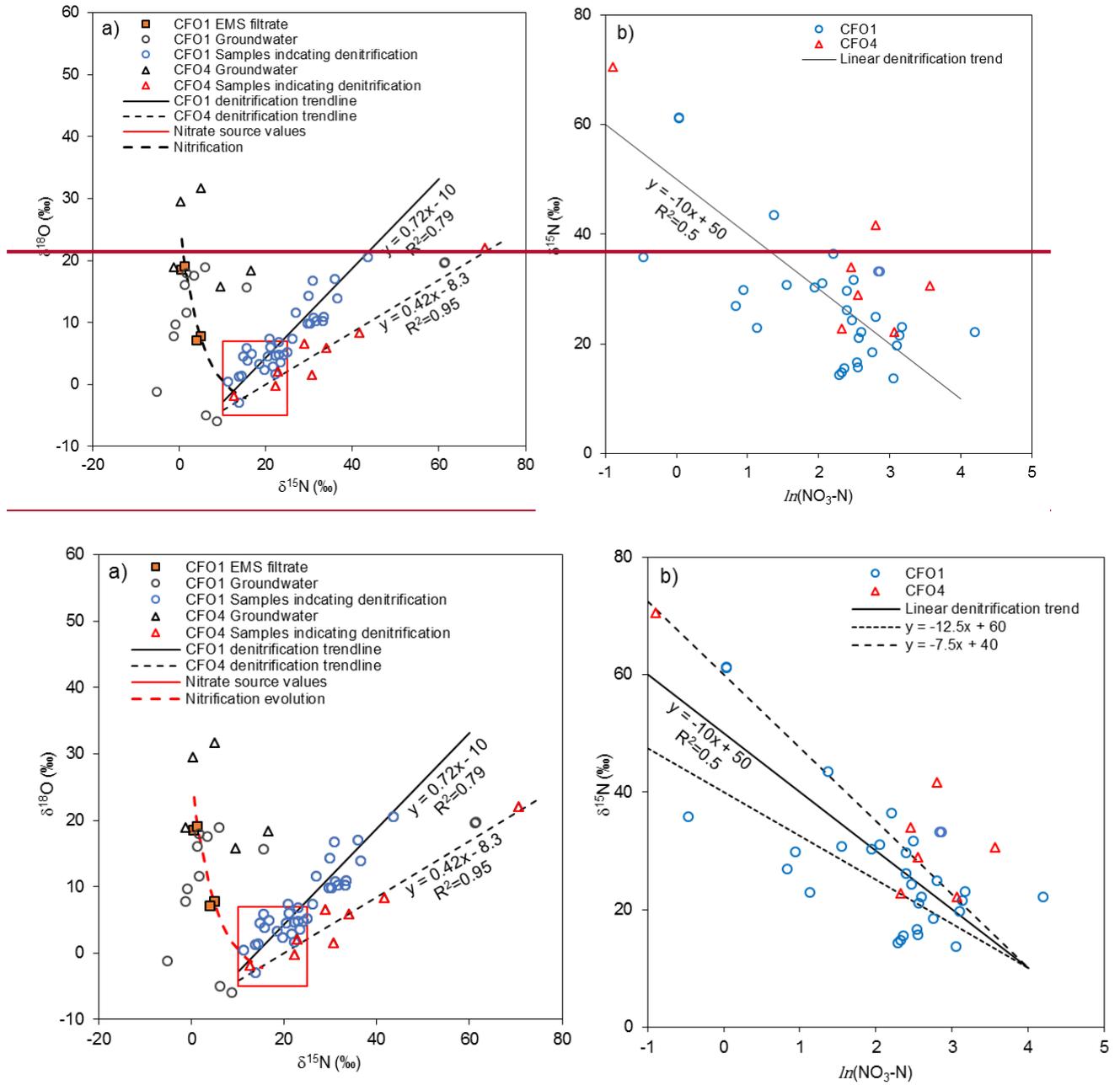
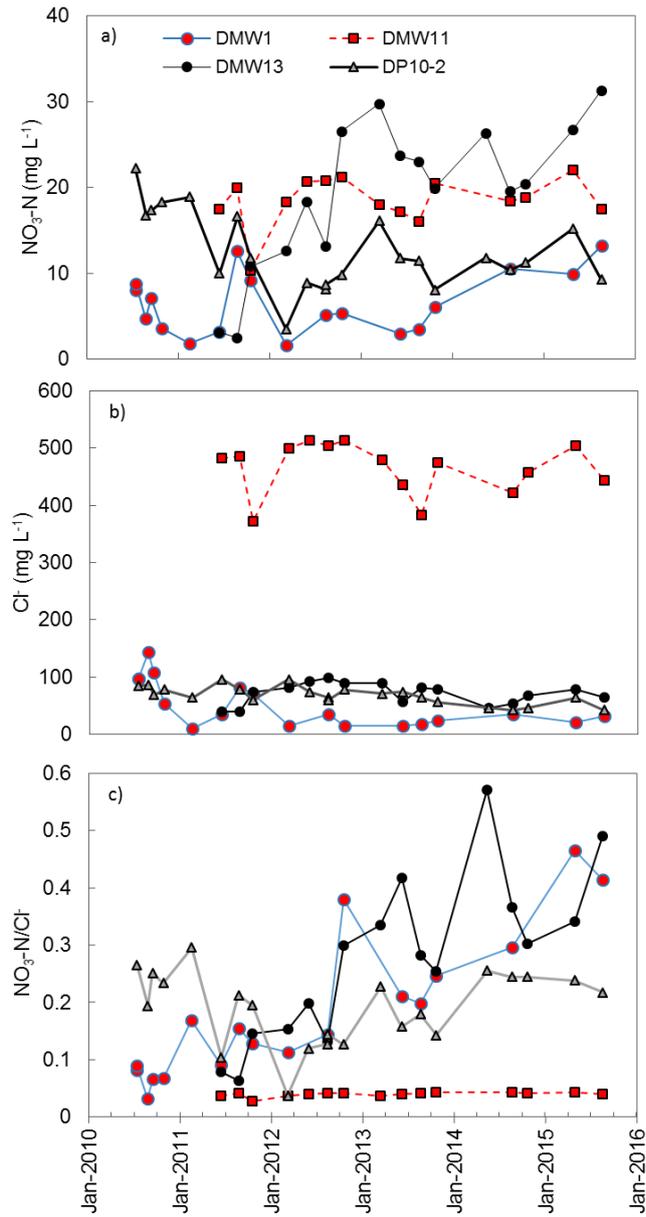
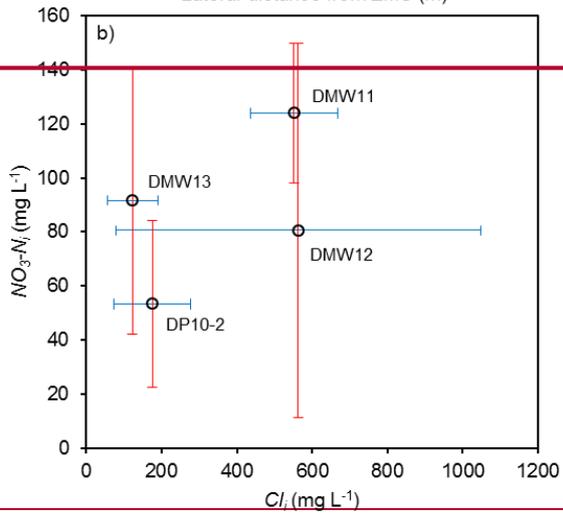
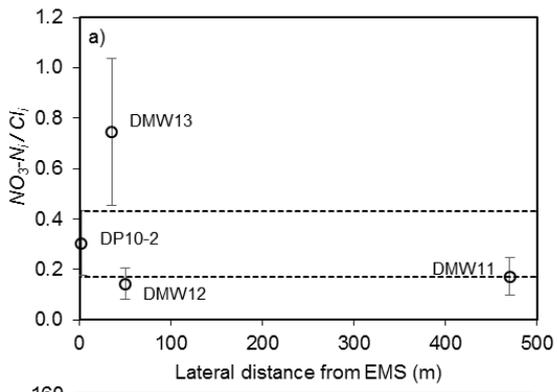


Figure 2 (a) Cross-plot of stable isotopes of nitrate at CFO1 and CFO4 showing hypothetical nitrification trend, boundary of manure-sourced  $\text{NO}_3^-$  values and linear enrichment trends associated with denitrification, (b) enrichment of  $\delta^{15}\text{N}_{\text{NO}_3}$  during denitrification (only samples within source region and with evidence of denitrification are shown) **dashed lines represent  $\pm 1$  std. dev. of enrichment factor ( $\epsilon = -10$ ) estimated from measured data.**

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**Figure 3** Temporal variations in (a)  $\text{NO}_3\text{-N}$ , (b)  $\text{Cl}^-$ , and (c)  $\text{NO}_3\text{-N}/\text{Cl}^-$  at CFO1. Only wells with  $\text{NO}_3\text{-N} > 10 \text{ mg L}^{-1}$  are shown.



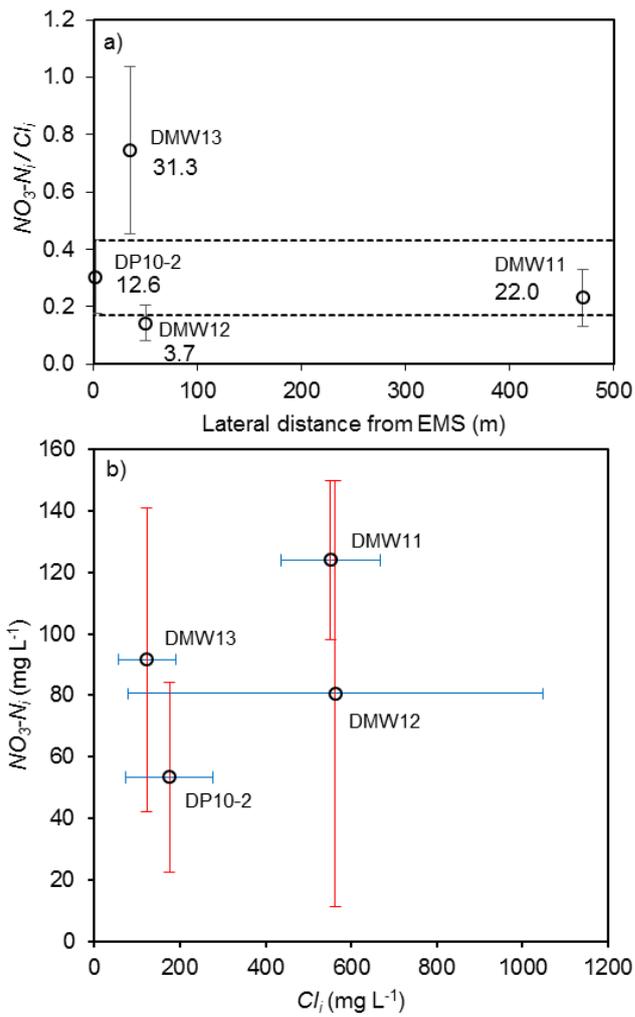


Figure 4 (a) Estimated  $NO_3-N_i/Cl_i$  ratios (mean and st. dev.) in water table wells with evidence of denitrification at CFO1, plotted with distance from earthen manure storage (EMS), where dashed lines are the upper and lower bounds of DP10-2 (EMS source), and (b) and values are maximum measured  $NO_3-N$  (mg L<sup>-1</sup>). (b) Estimated concentrations of  $NO_3-N_i$  and  $Cl_i$  at CFO1 (mid-range, error bars are max. and min. values).

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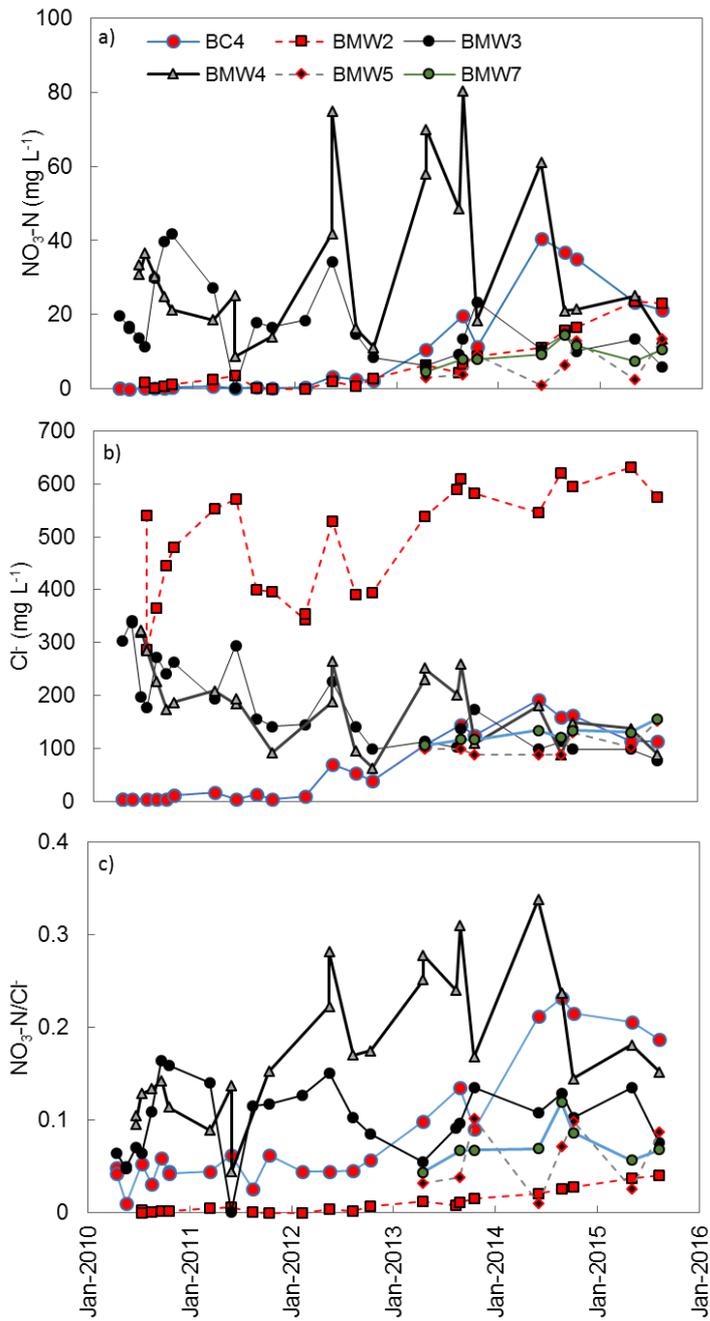
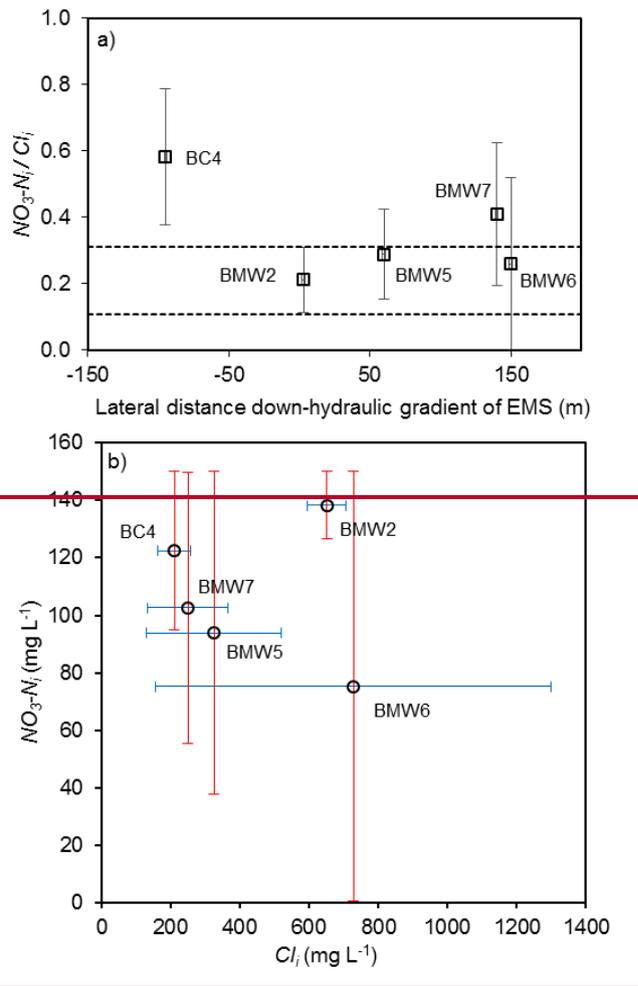


Figure 5 Temporal variations in (a)  $\text{NO}_3\text{-N}$ , (b)  $\text{Cl}^-$ , and (c)  $\text{NO}_3\text{-N}/\text{Cl}^-$  at CFO4. Only wells with  $\text{NO}_3\text{-N} > 10 \text{ mg L}^{-1}$  are shown.



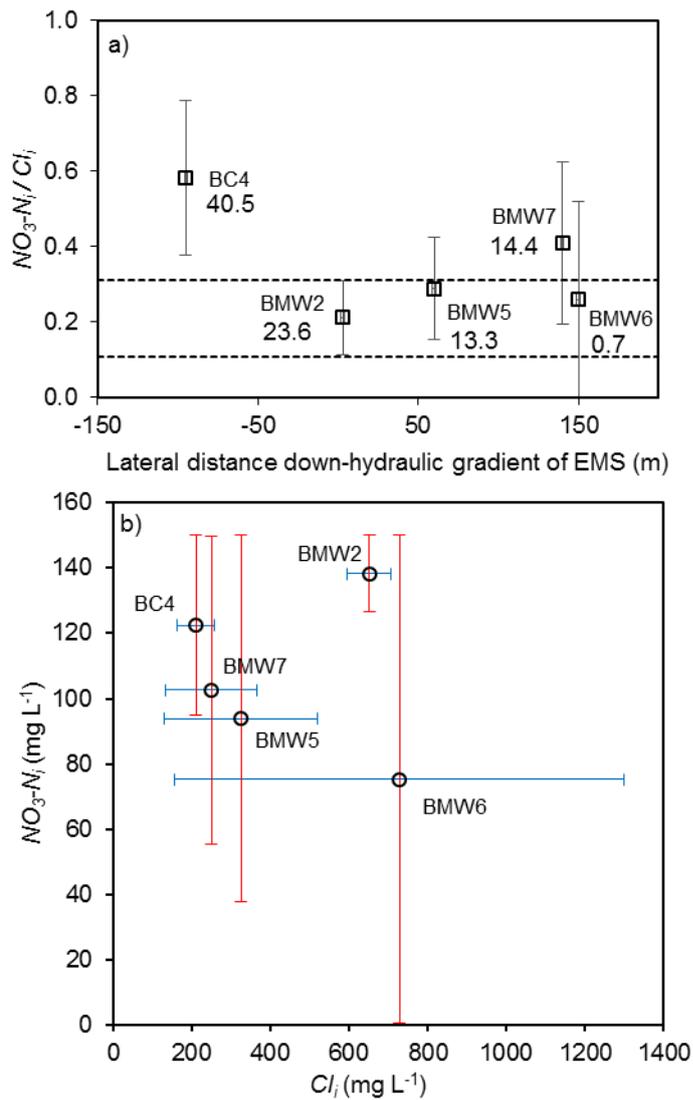
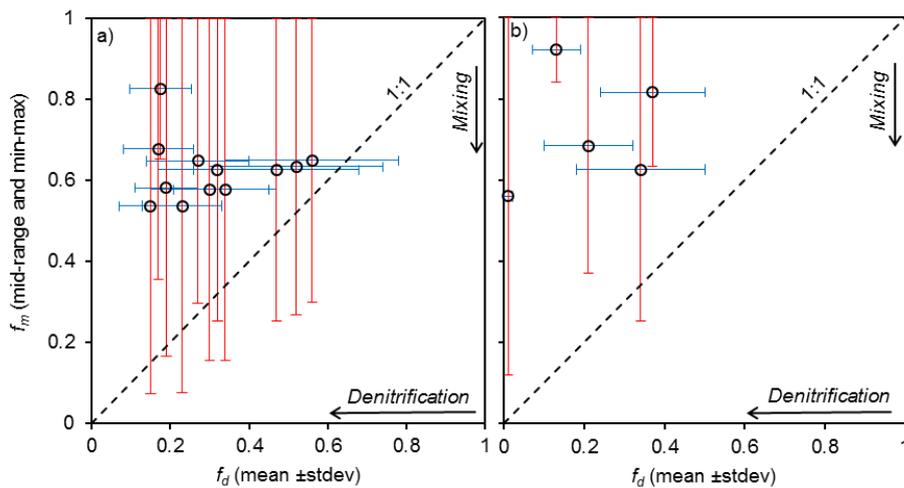


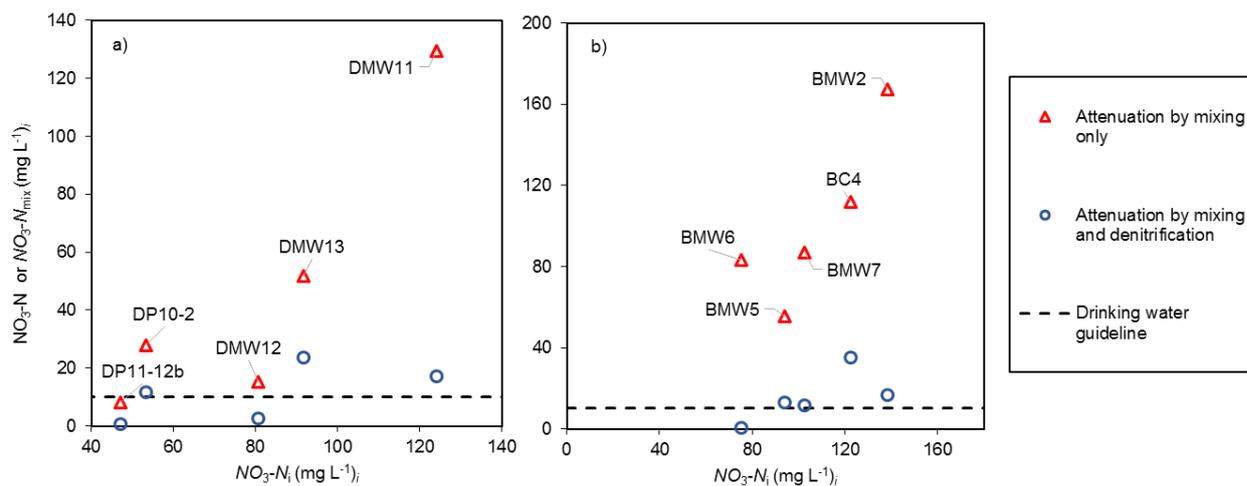
Figure 6 (a) Estimated  $NO_3-N_i/Cl_i$  ratios (mean and st. dev.) in water table wells with evidence of denitrification at CFO4, plotted with distance from earthen manure storage (EMS), where dashed lines are upper and lower bounds of BMW2 (EMS source) and values are maximum measured  $NO_3-N$  (mg L<sup>-1</sup>). (b) estimated concentrations of  $NO_3-N_i$  and  $Cl_i$  at CFO1 (mid-range, error bars are max. and min. values).

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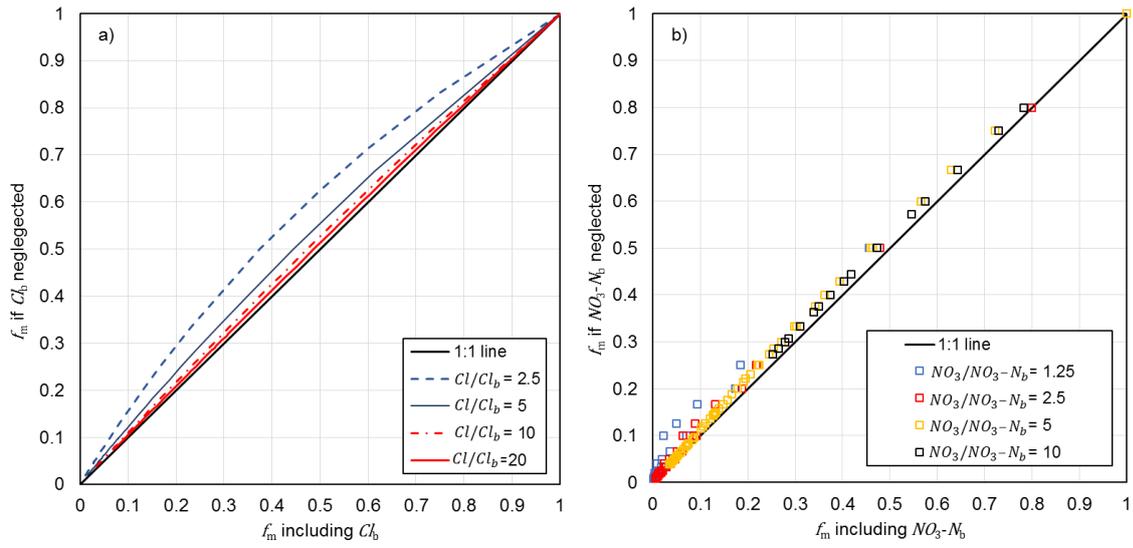
**Figure 7** Relative contributions to  $\text{NO}_3^-$  attenuation by mixing and denitrification, as indicated by estimated  $f_m$  and  $f_d$  at (a) CFO1 and (b) CFO4, for groundwater samples with denitrification indicated by stable isotope values of  $\text{NO}_3^-$ .

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**Figure 8** Measured concentrations of  $\text{NO}_3\text{-N}$  (blue circles - attenuation by mixing and denitrification) and  $\text{NO}_3\text{-N}_{\text{mix}}$  (red triangles - attenuation by mixing only) vs mid-range estimate of  $\text{NO}_3\text{-N}_i$  at a) CFO1 and b) CFO4. Dashed lines are drinking water guideline ( $10 \text{ mg L}^{-1}$  of  $\text{NO}_3\text{-N}$ ).

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**Figure 9 Effect of neglecting background concentrations ( $Cl_b$  or  $NO_3-N_b$ ) in the mixing model on calculated  $f_m$  over the range of values in this study.**

## Supplementary Material

### Measured hydraulic heads and gradients

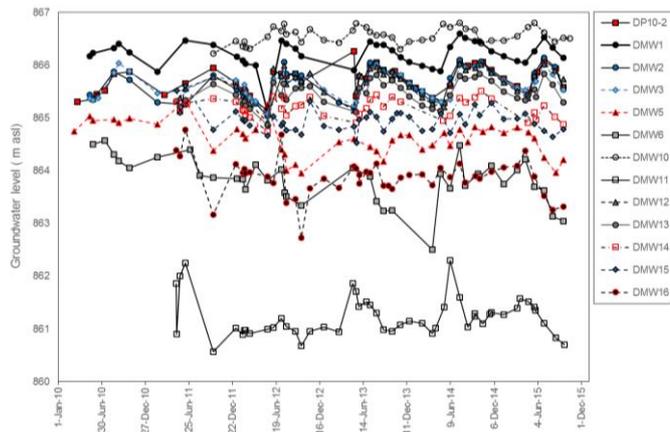


Figure S1. Time series of hydraulic heads measured in water table monitoring wells at CFO1

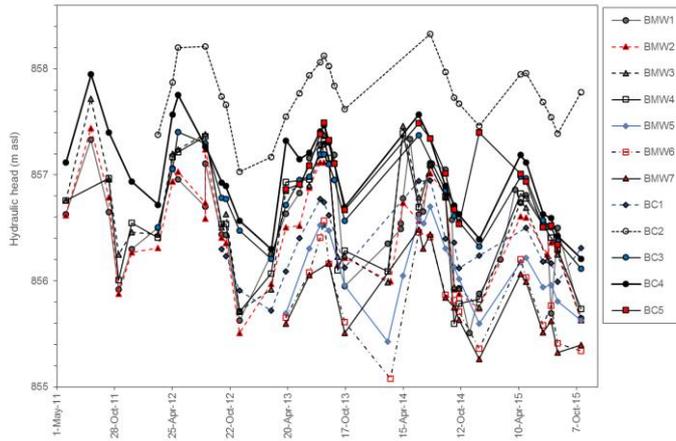


Figure S2. Time series of hydraulic heads measured in water table monitoring wells at CFO4

5 Table S1. Horizontal hydraulic gradients at CFO1 at the water table.

Well IDs	Horizontal hydraulic gradient
DMW1 and DP10-2	$4.63 \times 10^{-3}$
DMW2 and DMW-16	$6.06 \times 10^{-3}$
DP10-2 and DMW5	$4.39 \times 10^{-3}$
DP10-2 and DMW11	$9.74 \times 10^{-3}$
DMW10 and DMW11	$1.38 \times 10^{-2}$

**Table S2. Mean vertical gradients between nested water table wells and piezometers at CFO1**

Well IDs	Vertical hydraulic gradient
DMW10 and DP11-10b	$3.34 \times 10^{-3}$
DMW11 and DP11-11b	$-2.79 \times 10^{-2}$
DMW12 and DP11-12b	$2.20 \times 10^{-3}$
DMW13 and DP11-13b	$1.36 \times 10^{-2}$
DMW14 and DP11-14b	$1.80 \times 10^{-3}$
DMW15 and DP11-15b	$3.37 \times 10^{-2}$
DMW16 and DP11-16b	$2.86 \times 10^{-2}$
DP10-2 and DP10-1	$1.78 \times 10^{-1}$

**Table S3. Horizontal hydraulic gradients at CFO4 at the water table.**

Well IDs	Horizontal hydraulic gradient
BC2 and BMW2	$3.94 \times 10^{-3}$
BMW2 and BMW7	$4.32 \times 10^{-3}$
BC2 and BMW7	$3.79 \times 10^{-3}$

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**Table S4. Mean vertical hydraulic gradients in nested water table wells and piezometers at CFO4**

Well IDs	Vertical hydraulic gradient
BMW2 and BM10-15e	$4.61 \times 10^{-2}$
BMW4 and BP10-15w	$4.22 \times 10^{-2}$
BMW5 and BP5-15	$4.46 \times 10^{-2}$
BMW6 and BP6-15	$4.16 \times 10^{-2}$

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Measured hydrochemistry data

Table S5. Measured concentrations of chloride (Cl<sup>-</sup>), bicarbonate (HCO<sub>3</sub><sup>-</sup>), dissolved organic carbon (DOC), and ~~N-species~~ (total nitrogen (TN), NH<sub>3</sub>-N, NO<sub>3</sub>-N, NO<sub>2</sub>-N, and ~~TKN~~total organic nitrogen (TON)) in groundwater wells and water filtered from the EMS and catch basin at CFO1 (mean ± standard deviation).

Sample ID	Cl <sup>-</sup> (mg L <sup>-1</sup> )	HCO <sub>3</sub> <sup>-</sup> (mg L <sup>-1</sup> )	DOC (mg L <sup>-1</sup> )	NH <sub>3</sub> -N (mg L <sup>-1</sup> )	NO <sub>3</sub> -N* (mg L <sup>-1</sup> )	NO <sub>2</sub> -N (mg L <sup>-1</sup> )	<del>TKN</del> TON (mg L <sup>-1</sup> )	TN (mg L <sup>-1</sup> )
EMS filtrate	719 ±	5498 ±	1781 ± 1026	806 ± 303	<0.7-31 ±	-	-834 ± 408	1444 ± 364
	272552 ±	6802575 ±	1377 ± 948	512 ± 181	0.12	-	(n=7)	(n=7)
	63 (n=610)	457 (n=610)	(n=310)	(n=610)	(n=510)			
Catch basin filtrate	439 ±	979 ±	576 ± 408362	4.59 ± 3 ±	<0.51	-	-1023 ±	1027 ± 433
	322592 ±	937833 ±	(n=39)	2.1 (n=59)	(n=59)	-	433	(n=6)
	309 (n=59)	615 (n=59)					(n=6)	
DMW1	50 ± 40 (n=18)	453 ± 82 (n=18)	6.4 ± 1.4 (n=4)	<0.1 (n=18)	6.5 ± 3.6 (n=18)	<0.1 (n=18)	0.6 ± 0.2 (n=18)	7.2 ± 3.8 (n=18)
DMW2	404 ± 186 (n=20)	339 ± 61 (n=20)	3.5 ± 0.5 (n=5)	0.1 ± 0 (n=20)	1.2 ± 1.3 (n=20)	<0.1 (n=20)	2.9 ± 0.5 ± 0.62 (n=2017)	3.2 ± 0.2 (n=17)
DMW3	871 ± 146 (n=22)	4362 ± 476 (n=22)	282.1 ± 30 (n=5)	373.4 ± 79.4 (n=22)	1.1 ± 2.7 (n=22)	2.7 ± 8.3 (n=22)	424.14 ± 0 ± 73.6.7 (n=2216)	20.2 ± 3.2 (n=16)
DMW4	50 ± 24 (n=21)	448 ± 57 (n=21)	4.5 ± 0.8 (n=5)	0.2 ± 0.7 (n=5)	0.1 ± 0.2 (n=21)	<0.1 (n=21)	0.5 ± 1.3 ± 0.1 (n=2116)	3.2 ± 0.5 (n=16)
DMW5	35 ± 11 (n=22)	534 ± 30 (n=22)	6.6 ± 1.0 (n=5)	0.1 ± 0.1 (n=22)	1.0 ± 0.5 (n=22)	<0.1 (n=22)	0.49 ± 0.47 (n=2216)	21.2 ± 9.0 (n=16)
DMW6	394 ± 25 (n=21)	778 ± 67 (n=21)	25.8 ± 5.4 (n=5)	4.0 ± 1.0 (n=21)	0.2 ± 0.2 (n=21)	<0.1 (n=21)	6.6 ± <0.91 (n=2115)	0.4 ± 0.2 (n=15)
DMW10	234 ± 7 (n=17)	712 ± 15 (n=17)	58.5 ± 1.0 (n=5)	0.2 ± 0.1 (n=17)	0.1 ± 0.2 (n=17)	0.1 ± 0 (n=17)	<0.1 (n=16)	3.4 ± <0.43 (n=1716)
DMW11	437 ± 121 (n=16)	771 ± 38 (n=16)	18.0 ± 1.7 (n=5)	0.3 ± 0.2 (n=16)	18.5 ± 2.7 (n=16)	0.1 ± 0.3 (n=16)	1.6 ± 0.83 ± 0.1 (n=16)	0.5 ± 0.2 (n=16)
DMW12	75 ± 11 (n=16)	405 ± 24 (n=16)	3.9 ± 0.6 (n=5)	0.1 ± 0.1 (n=16)	2.8 ± 0.5 (n=16)	0.1 ± 0 (n=16)	0.34 ± 0.26 (n=1620)	1.7 ± 1.6 (n=20)
DMW13	70 ± 19 (n=16)	767 ± 119 (n=16)	7.7 ± 1.7 (n=5)	0.9 ± 1.0 (n=16)	19.2 ± 8.7 (n=16)	0.2 ± 0.2 (n=16)	50.6 ± 17.2 (n=22)	1427.8 ± 1469.2 (n=1622)
DMW14	7 ± 5 (n=15)	445 ± 66 (n=15)	3.7 ± 0.6 (n=5)	0.3 ± 0.1 (n=15)	<0.1 (n=15)	<0.1 (n=15)	0.3 ± 0.26 (n=1521)	0.6 ± 1.5 (n=21)
DMW15	14 ± 1 (n=16)	670 ± 32 (n=16)	3.8 ± 0.9 (n=5)	0.1 ± 0 (n=16)	<0.1 (n=16)	<0.1 (n=16)	<0.2 3 ± 0.1 (n=1622)	1.5 ± 0.4 (n=22)
DMW16	65 ± 7 (n=16)	604 ± 18 (n=16)	7.3 ± 0.5 (n=5)	<0.1 (n=16)	0.1 ± 0.1 (n=16)	<0.1 (n=16)	2.6 ± 0.3 ± 0.48 (n=1621)	6.9 ± 0.9 (n=21)
DP10-1	<5 (n=23)	467 ± 19 (n=23)	3.7 ± 0.5 (n=5)	0.7 ± 0.1 (n=23)	<0.1 (n=23)	<0.1 (n=23)	10.3 ± 0.5 (n=23)	1.2 ± 0.5 (n=23)
DP10-2	68 ± 16 (n=22)	701 ± 36 (n=22)	6.3 ± 1.1 (n=5)	1.2 ± 0.9 (n=22)	12.6 ± 4.5 (n=22)	0.1 ± 0.1 (n=22)	2.1 ± 0.9 ± 0.5 (n=22)	14.8 ± 4.2 (n=22)
DP11-10b	22 ± 14 (n=17)	689 ± 102 (n=17)	30.3 ± 24.9 (n=5)	0.5 ± 0.1 (n=17)	0.5 ± 1.7 (n=17)	<0.1 (n=17)	0.72 ± 0.2 (n=17)	1.3 ± 1.6 (n=17)
DP11-11b	16 ± 3 (n=16)	604 ± 67 (n=16)	8.9 ± 2.2 (n=5)	1.2 ± 0 (n=16)	<0.1 (n=16)	<0.1 (n=16)	1.3 ± <0.1 (n=16)	1.4 ± 0.1 (n=16)

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DP11-12b	98 ± 20 (n=15)	492 ± 23 (n=15)	6.5 ± 0.6 (n=5)	0.1 ± 0.1 (n=15)	1.4 ± 1.3 (n=15)	<0.1 (n=15)	0.54 ± 0.1 (n=15)	1.9 ± 1.3 (n=15)
DP11-13b	15 ± 3 (n=16)	436 ± 26 (n=16)	11.7 ± 4.2 (n=5)	0.7 ± 0 (n=16)	<0.1 (n=16)	<0.1 (n=16)	0.92 ± 0.1 (n=16)	1.0 ± 0.1 (n=16)
DP11-14b	6 ± 3 (n=16)	461 ± 47 (n=16)	7.3 ± 1.1 (n=5)	0.9 ± 0.1 (n=16)	<0.1 (n=16)	<0.1 (n=16)	<del>0.1</del> 0 ± 0.1 (n=16)	1.1 ± 0.1 (n=16)
DP11-15b	6 ± 2 (n=17)	442 ± 91 (n=17)	6.4 ± 2.6 (n=6)	0.7 ± 0.1 (n=17)	<0.1 (n=17)	<0.1 (n=17)	<del>0.8 ± 0.2</del> 1 (n=17)	0.9 ± 0.2 (n=17)
DP11-16b	33 ± 3 (n=17)	531 ± 55 (n=17)	9.0 ± 8.4 (n=5)	0.8 ± 0.1 (n=17)	<0.1 (n=17)	≤ 0.1 ± 0 (n=17)	0.9 ± 0.1 (n=17)	1.0 ± 0.1 (n=17)

\*For EMS filtrate and catch basin filtrate, these values are NO<sub>3</sub>-N + NO<sub>2</sub>-N

**Table S6. Measured concentrations of chloride (Cl<sup>-</sup>), bicarbonate (HCO<sub>3</sub><sup>-</sup>), dissolved organic carbon (DOC), and N-species (total nitrogen (TN), NH<sub>3</sub>-N, NO<sub>3</sub>-N, NO<sub>2</sub>-N, and ~~TKN~~ total organic nitrogen (TON)) in groundwater wells and water filtered from the EMS at CFO4 (mean ± standard deviation).**

Sample ID	Cl <sup>-</sup> (mg L <sup>-1</sup> )	HCO <sub>3</sub> <sup>-</sup> (mg L <sup>-1</sup> )	DOC (mg L <sup>-1</sup> )	NH <sub>3</sub> -N (mg L <sup>-1</sup> )	NO <sub>3</sub> -N* (mg L <sup>-1</sup> )	NO <sub>2</sub> -N (mg L <sup>-1</sup> )	<del>TKN</del> TON (mg L <sup>-1</sup> )	TN (mg L <sup>-1</sup> )
EMS filtrate	<del>4074 ± 17</del> 379806 ± 17 (n=23)	<del>5795 ± 89</del> 15442353 ± 89 (n=23)	3367 ± 115 (n=43)	<del>865 ± 12</del> 182736 ± 12 (n=23)	<0.7-27 ± 0.02 (n=23)	-	<del>407 ± 118</del> (n=3)	1143 ± 127 (n=3)
BC1	<10 (n=11)	494 ± 13 (n=11)	5.0 ± 0.8 (n=4)	<0.1 (n=11)	<0.1 (n=11)	<0.1 (n=11)	<0.2 1 (n=11)	<0.3 (n=11)
BC2	6 ± 3 (n=12)	516 ± 33 (n=12)	6.0 ± 3.0 (n=4)	<0.1 (n=12)	1.1 ± 2.7 (n=12)	<0.1 (n=12)	0.32 ± 0.2 (n=12)	1.4 ± 2.8 (n=12)
BC3	<5 (n=13)	504 ± 21 (n=13)	6.9 ± 2.9 (n=4)	<0.1 (n=13)	0.1 ± 0.1 (n=13)	<0.1 (n=13)	0.21 ± 0.1 (n=13)	<0.3 (n=13)
BC4	58 ± 64 (n=24)	576 ± 110 (n=24)	9.2 ± 3.5 (n=9)	<0.1 (n=24)	8.8 ± 13.2 (n=24)	<0.1 (n=24)	0.87 ± 0.8 (n=24)	9.6 ± 14.0 (n=24)
BC5	26 ± 6 (n=8)	498 ± 51 (n=8)	6.8 ± 3.1 (n=3)	<0.1 (n=8)	5.7 ± 1.5 (n=8)	<0.1 (n=8)	0.6 ± 0.4 (n=8)	6.3 ± 1.5 (n=8)
BMW1	305 ± 251 (n=28)	926 ± 190 (n=28)	21.5 ± 12.4 (n=11)	<0.1 (n=28)	2.2 ± 2.5 (n=28)	<0.1 (n=28)	1.1 ± 0.9 (n=28)	3.3 ± 3.2 (n=28)
BMW2	502 ± 97 (n=22)	1186 ± 87 (n=22)	20.2 ± 4.9 (n=9)	<0.1 (n=22)	6.0 ± 7.4 (n=22)	0.1 ± 0.1 (n=22)	1.76 ± 0.4 (n=22)	7.8 ± 7.6 (n=22)
BMW3	182 ± 81 (n=25)	881 ± 146 (n=25)	15.6 ± 3.3 (n=9)	<0.1 (n=25)	17.4 ± 10.3 (n=25)	0.1 ± 0.1 (n=25)	1.6 ± 0.8 (n=25)	19.1 ± 10.8 (n=25)
BMW4	188 ± 74 (n=24)	666 ± 55 (n=24)	12.0 ± 3.3 (n=11)	<0.1 (n=24)	33.6 ± 21.1 (n=24)	0.2 ± 0.3 (n=24)	2.65 ± 2.9 (n=24)	36.3 ± 21.9 (n=24)
BMW5	106 ± 23 (n=8)	975 ± 163 (n=8)	8.6 ± 1.3 (n=3)	<0.1 (n=8)	6.5 ± 4.8 (n=8)	0.1 ± 0 (n=8)	0.7 ± 0.3 (n=8)	7.3 ± 4.9 (n=8)
BMW6	156 ± 18 (n=8)	538 ± 27 (n=8)	6.9 ± 1.7 (n=3)	<0.1 (n=8)	0.4 ± 0.2 (n=8)	0.1 ± 0 (n=8)	0.5 ± 0.1 (n=8)	1.0 ± 0.2 (n=8)
BMW7	127 ± 15 (n=8)	699 ± 65 (n=8)	8.1 ± 2.8 (n=3)	<0.1 (n=8)	9.2 ± 3.0 (n=8)	0.1 ± 0 (n=8)	0.7 ± 0.4 (n=8)	10.0 ± 3.2 (n=8)
BP10-15e	7 ± 4 (n=19)	493 ± 33 (n=19)	3.4 ± 0.4 (n=7)	0.1 ± 0.1 (n=19)	0.1 ± 0.1 (n=19)	<0.1 (n=19)	0.2 ± 0.1 (n=19)	0.4 ± 0.2 (n=19)

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BP10-15w	<5 (n=17)	507 ± 11 (n=17)	3.5 ± 0.6 (n=4)	<0.2 (n=17)	0.3 ± 1.0 (n=17)	<0.1 (n=17)	0.2 ± <0.1 (n=17)	0.6 ± 1.1 (n=17)
BP5-15	<5 (n=8)	509 ± 12 (n=8)	5.0 ± 1.1 (n=3)	<0.1 (n=8)	<0.1 (n=8)	<0.1 (n=8)	<0.2 1 (n=8)	<0.3 (n=8)
BP6-15	<5 (n=7)	487 ± 7 (n=7)	3.3 ± 1.1 (n=3)	<0.2 (n=7)	<0.1 (n=7)	<0.1 (n=7)	<0.2 1 (n=7)	<0.3 (n=7)

\*For EMS filtrate, this value is NO<sub>3</sub>-N + NO<sub>2</sub>-N

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Table S7. Hydrochemistry of water from continuous core samples

Core ID	Depth (m BG)	Lithology	Cl- (mg L <sup>-1</sup> )	NH <sub>3</sub> -N (mg L <sup>-1</sup> )	NO <sub>3</sub> -N (mg L <sup>-1</sup> )	NO <sub>2</sub> -N (mg L <sup>-1</sup> )	NO <sub>3</sub> -N/Cl-
DC15-20	2	Sand	76.4	4.27	0.64	4.99	0.008
	3	Sand	47.2	2.02	2.42	3.75	0.051
	4	Sand	22.3	2.45	1.76	0.12	0.079
	5	Sand	21.0	1.88	0.96	0.07	0.046
	6	Sand	28.2	2.12	1.16	0.14	0.041
	7	Sand	27.2	2.19	0.89	0.33	0.033
	8	Sand	28.5	2.85	14.39	0.32	0.505
	9	Sand	12.9	1.29	0.68	1.39	0.053
	10	Sand	35.7	1.95	2.05	0.81	0.057
	10.5	Sand	33.0	0.00	4.10	0.00	0.124
	11	Sand	64.1	2.17	1.38	1.23	0.022
	12	Sand	112.4	2.17	2.12	0.03	0.019
	13	Sand	119.8	1.70	2.77	0.30	0.023
	14	Sand	75.6	1.06	0.85	2.20	0.011
	15	Sand	56.3	2.30	2.04	0.00	0.036
DC15-21	2	Sand	147.6	1.37	0.14	1.83	0.001
	2.5	Sand	23.7	0.82	0.90	0.29	0.038
	3.5	Sand	18.0	1.29	3.72	1.78	0.207
	4.5	Sand	20.5	1.91	4.74	0.26	0.232
	5	Sand	29.7	1.24	3.59	0.00	0.121
	6	Sand	22.8	2.00	0.95	0.04	0.042
	7	Sand	33.6	2.98	1.93	0.25	0.058
	8	Sand	24.4	1.67	4.07	0.16	0.167
	9	Sand	25.6	3.26	3.65	0.08	0.142
	10	Sand	21.5	0.82	1.28	0.21	0.060
DC15-22	2	Sand	72.9	1.19	13.44	0.00	0.184
	2.5	Clay	72.8	0.84	17.52	3.73	0.241
	3	Sand	79.8	0.76	16.66	0.12	0.209
	4	Sand	109.8	1.94	22.88	1.28	0.208
	5	Sand	60.8	2.59	12.82	2.17	0.211
	6.5	Sand	99.2	3.20	4.68	4.04	0.047
	7	Sand	88.4	2.40	9.90	0.00	0.112
	7	Sand	95.0	0.00	6.08	2.80	0.064
	8	Sand	75.8	1.92	12.89	0.00	0.170
	9.5	Sandy clay	157.7	1.54	39.50	2.04	0.251
	10	Sandy clay	73.0	1.55	10.99	0.29	0.151
	11	Sand	107.7	3.32	12.10	0.82	0.112
12	Sand	91.4	1.14	15.60	1.45	0.171	
DC15-23	2	Clay	70.0	0.94	66.40	1.35	0.948
	3	Clay	122.2	0.76	9.48	1.87	0.078
	4	Clay	48.8	5.87	8.90	0.86	0.182
	5	Clay	56.1	4.62	10.53	0.63	0.188
	6	Sand	98.2	8.59	7.05	1.87	0.072

6.5	Sand	61.2	1.86	9.76	2.93	0.160
7	Sand	84.9	1.57	10.17	0.25	0.120
7.5	Sand	57.5	2.60	10.51	0.06	0.183
8	Sand	67.8	2.24	9.88	1.13	0.146
8.5	Clay	106.1	9.82	7.47	0.31	0.070
9	Sand	85.5	11.70	12.69	0.92	0.148
9.5	Sand	72.4	9.75	17.27	1.85	0.238
11	Sand	82.6	9.20	21.05	0.07	0.255
11.5	Sand	68.5	2.99	20.88	1.02	0.305
12	Clay	87.9	0.69	1.52	2.06	0.017
13	Clay	22.9	5.07	1.01	0.00	0.044
14	Clay	17.9	1.80	1.16	0.34	0.065
15	Clay	12.6	1.47	1.01	0.32	0.080

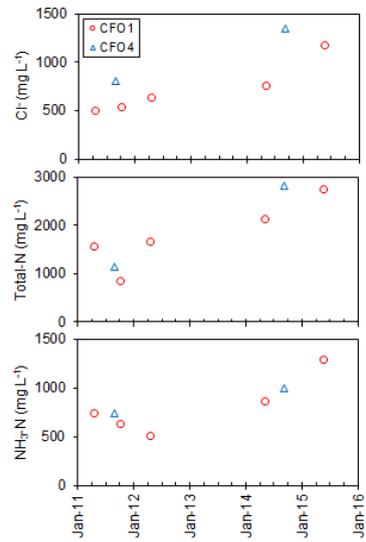
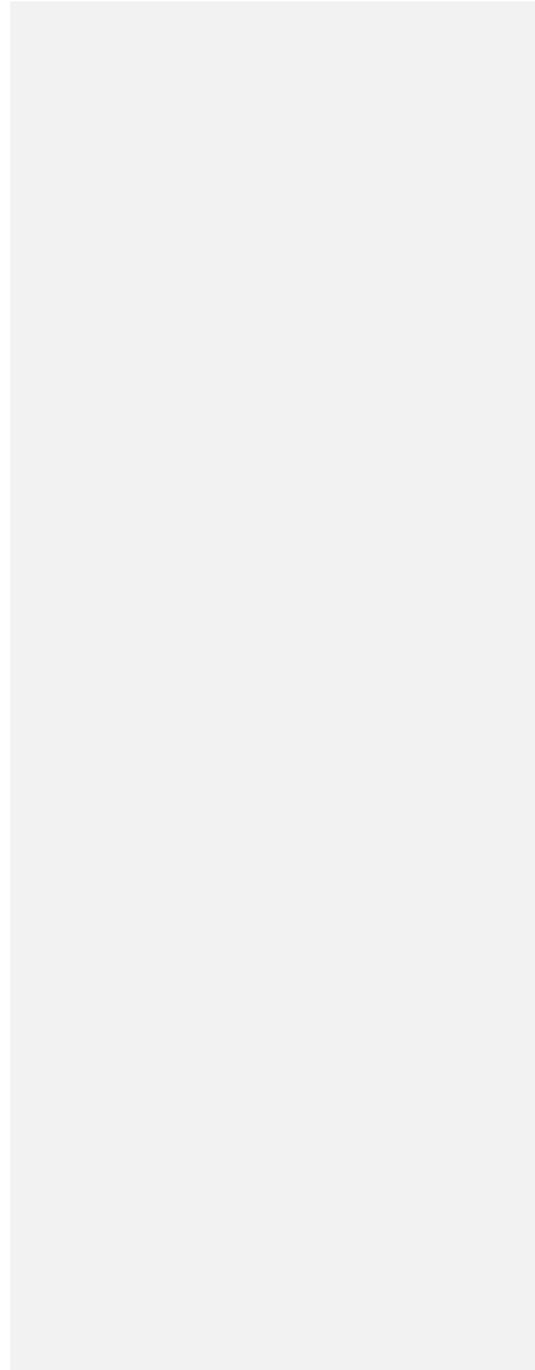


Figure S3. Concentrations of Cl<sup>-</sup>, total-N, and NH<sub>4</sub>-N in water filtered from the EMS slurry at CFO1 and CFO4.

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### Stable isotopes of water and nitrate

Samples for the stable isotopes of water ( $\delta^2\text{H}$  and  $\delta^{18}\text{O}_{\text{H}_2\text{O}}$ ) were collected from wells at CFO1 quarterly between February 2011 and August 2013. Samples for stable isotopes of water were collected from wells at CFO4 on 16 October 2013. Wells were purged prior to sample collection (1–3 casing volumes) in 20 mL HDPE bottles. Core samples for analysis of stable isotopes of water were stored in Ziploc™ bags and kept cool until analysis.

Stable isotopes of water ( $\delta^2\text{H}$  and  $\delta^{18}\text{O}_{\text{H}_2\text{O}}$ ) in groundwater samples from wells and pore water squeezed from continuous core were analyzed using a Los Gatos LGR model 908-0008 liquid water isotope analyzer (off-axis integrated cavity output spectroscopy) (Lis et al., 2008). The accuracy of this method is  $\pm 0.8\text{‰}$  for  $\delta^2\text{H}$  and  $\pm 0.1\text{‰}$  for  $\delta^{18}\text{O}_{\text{H}_2\text{O}}$ . Pore water from continuous core collected in 2015 was analyzed for  $\delta^2\text{H}$  and  $\delta^{18}\text{O}_{\text{H}_2\text{O}}$  using the vapour equilibration method (Wassenaar et al. (2008). The Ziploc bag containing the core sample was filled with dry air to equilibrate with the pore water vapour for 3 days at room temperature. The isotopic values of this equilibrated vapour was then analyzed using a Picarro L1102-*i* water isotope analyzer. The precision of this analysis is  $\pm 2.0\text{‰}$  for  $\delta^2\text{H}$  and  $\pm 4.0\text{‰}$  for  $\delta^{18}\text{O}_{\text{H}_2\text{O}}$ . Stable isotopic values of ground water were predominantly close to Calgary meteoric water line (Peng et al., 2004) with  $\delta^2\text{H}_{\text{H}_2\text{O}}$  ranging from -175.9 to 117.2‰ and  $\delta^{18}\text{O}_{\text{H}_2\text{O}}$  ranging from -22.5 to -12.9‰.

**Table S8. Stable isotope values of water and nitrate at CFO1**

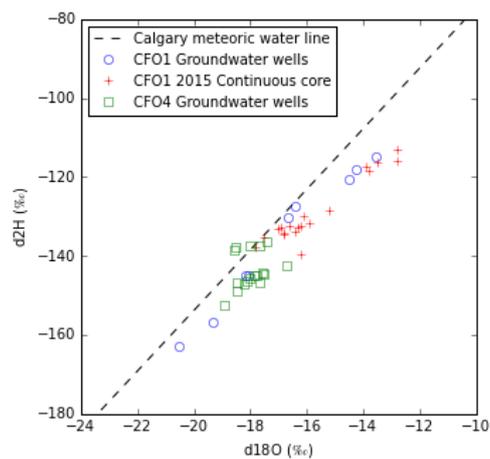
Site	Well ID*	$\delta^{18}\text{O}_{\text{H}_2\text{O}}$	$\delta^2\text{H}_{\text{H}_2\text{O}}$	$\delta^{18}\text{O}_{\text{NO}_3}$	$\delta^{15}\text{N}_{\text{NO}_3}$
CFO1†	DMW1	-16.7 ± 1.3 (n=4)	-136.2 ± 10.3 (n=4)	-0.5 ± (n=1)	12.6 ± (n=1)
	DMW2	-15.5 ± 0.6 (n=7)	-126.9 ± 4.4 (n=7)	6.0 ± 2.0 (n=2)	20.6 ± 0.3 (n=2)
	DMW3	-13.8 ± 0.5 (n=9)	-118.2 ± 0.8 (n=9)	-1.2 (n=1)	7.8 (n=1)
	DMW4	-14.2 ± 0.4 (n=7)	-119.9 ± 0.9 (n=7)	-	-
	DMW5	-14.9 ± 0.5 (n=7)	-124.1 ± 1.8 (n=7)	19.7 ± 0.1 (n=2)	61.3 ± 0.1 (n=2)
	DMW6	-15.2 ± 0.2 (n=7)	-126.8 ± 0.9 (n=7)	-	-
	DMW10	-17.8 ± 0.2 (n=8)	-143.6 ± 0.9 (n=8)	-	-
	DMW11	-16.6 ± 0.2 (n=7)	-134.6 ± 1.1 (n=7)	10.6 ± 0.4 (n=2)	33.2 ± 0.1 (n=2)
	DMW12	-15.7 ± 0.3 (n=7)	-127.7 ± 0.5 (n=7)	13.0 ± 1.9 (n=2)	28.4 ± 2.1 (n=2)
	DMW13	-16.1 ± 0.6 (n=7)	-127.7 ± 3.4 (n=7)	5.8 ± 1.4 (n=2)	23.0 ± 0.1 (n=2)
	DMW14	-14.5 ± 0.6 (n=7)	-121.7 ± 2.4 (n=7)	-	-
	DMW15	-15.0 ± 0.2 (n=8)	-125.5 ± 1.1 (n=8)	-	-
	DMW16	-15.4 ± 0.3 (n=7)	-128.5 ± 1.2 (n=7)	-	-
	DP10-1	-18.0 ± 0.7 (n=9)	-145.8 ± 2.4 (n=9)	11.5 (n=1)	1.6 ± (n=1)
	DP10-2	-16.8 ± 0.3 (n=9)	-131.8 ± 2.6 (n=9)	3.6 ± 1.8 (n=2)	22.0 ± 3.2 (n=2)
	DP11-10b	-19.1 ± 0.3 (n=8)	-152.9 ± 0.7 (n=8)	-	-
DP11-11b	-21.6 ± 0.3 (n=7)	-171.0 ± 0.8 (n=7)	-	-	
DP11-12b	-15.4 ± 0.5 (n=7)	-126.0 ± 1.3 (n=7)	18.8 ± 2.5 (n=2)	39.7 ± 5.4 (n=2)	
DP11-13b	-18.3 ± 0.2 (n=7)	-146.7 ± 1.2 (n=7)	-	-	
DP11-14b	-21.1 ± 0.4 (n=9)	-165.7 ± 2.2 (n=9)	-	-	
DP11-15b	-22.2 ± 0.3 (n=8)	-174.0 ± 1.0 (n=8)	-	-	
DP11-16b	-20.8 ± 0.4 (n=7)	-163.6 ± 0.7 (n=7)	-	-	
EMS filtrate			13.1 ± 6.5 (n=4)	2.6 ± 2.1 (n=4)	
	DP11-13_4m		9.8	30.3	
	DP11-13_5m		10.8	31.0	
	DP11-13_6m		5.2	24.5	
	DP11-13_7m		10.2	31.6	
	DP11-13_8m		14.0	36.4	
	DP11-13_9m		9.9	29.6	
	C15-20_3m	-116.0	-12.8	9.7	-0.9
	C15-20_8m	-117.2	-13.9	-1.2	-5.2
	C15-20_13m	-118.4	-13.8	16.0	1.3
	C15-21_2m	-116.1	-13.5	3.6	23.3
	C15-21_8m	-113.0	-12.8	-4.9	6.2
	C15-22_2m	-130.0	-16.1	4.7	22.2
	C15-22_4m	-128.3	-15.2	2.8	21.6
	C15-22_5m	-134.3	-16.8	3.9	15.7
	C15-22_6.5m	-134.0	-16.4	16.8	30.8
	C15-22_8m	-135.3	-17.5	5.6	21.1
	C15-22_10m	-132.6	-16.9	7.4	26.1
	C15-22_12m	-133.2	-17.0	3.3	18.5
	C15-23_2m	-134.7	-16.8	1.7	22.1
	C15-23_5m	-137.6	-17.8	5.9	15.6
	C15-23_7m	-132.5	-16.2	4.6	14.8
	C15-23_8m	-132.3	-16.6	1.46	14.3
	C15-23_9m	-132.7	-16.3	4.9	16.7
	C15-23_11m	-131.8	-15.9	1.3	13.7
	C15-23_13m	-139.4	-16.2	15.7	15.6

† For all continuous core samples n=1. \*central depth of core samples, x, indicated as SampleID\_xm

**Table S9. Stable isotope values of water and nitrate at CFO4**

Site	Well ID	$\delta^{18}\text{O}_{\text{H}_2\text{O}}$	$\delta^2\text{H}_{\text{H}_2\text{O}}$	$\delta^{18}\text{O}_{\text{NO}_3}$	$\delta^{15}\text{N}_{\text{NO}_3}$
CFO4†	BC1	-16.7	-142.3	29.5	0.3
	BC2	-18.6	-138.6	15.8	9.4
	BC3	-17.5	-144.6	31.6	5.0
	BC4	-18.5	-148.8	1.6	30.6
	BC5	-18.5	-137.6	-1.9	12.6
	BMW1	-17.6	-144.1	-	-
	BMW2	-17.4	-136.5	8.3	41.6
	BMW3	-	-	2.1	22.8
	BMW4	-18.0	-145.6	-0.3	22.2
	BMW5	-18.0	-137.5	6.5	28.9
	BMW6	-18.9	-152.4	22.1	70.5
	BMW7	-	-	5.9	34.0
	BP10-15e	-18.1	-146.5	18.3	16.4
	BP10-15w	-	-	18.9	-1.3
	BP5-15	-17.7	-137.3	-	-
	BP6-15	-17.9	-145.1	-	-

† For all samples at CFO4 n=1.



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**Figure S4. Cross-plot of stable isotopic values of groundwater wells at CFO1 and CFO4 and continuous core samples collected at CFO1 during 2015, relative to the Calgary meteoric water line ( $\delta^2\text{H} = 7.68 \delta^{18}\text{O}_{\text{H}_2\text{O}} - 0.21$ ).**

**Table S10 Constraining values and results of mixing model calculations**

Sample ID	Cl	NO <sub>3</sub> -N	f <sub>d</sub>	NO <sub>3</sub> -N <sub>i</sub> /Cl <sub>i</sub>	Cl <sub>i</sub> (mg L <sup>-1</sup> )		NO <sub>3</sub> -N <sub>i</sub> (mg L <sup>-1</sup> )		f <sub>m</sub>	
	(mg L <sup>-1</sup> )	(mg L <sup>-1</sup> )	(mean ± stdev)	(mean ± stdev)	min	max	min	max	min	max
<b>CFO1</b>										
DMW11	436.1	17.1	0.17 ± 0.07	0.23 ± 0.10	436	667	98	150	0.65	1
DMW12	78.0	2.6	0.23 ± 0.10	0.14 ± 0.06	78	1047	11	150	0.07	1
DMW13	56.7	23.7	0.56 ± 0.22	0.75 ± 0.29	57	189	42	141	0.30	1
DP10-2	74.5	11.8	0.52 ± 0.22	0.30 ± 0.13	74	277	23	84	0.27	1
DP11-12b	95.7	0.6	0.15 ± 0.08	0.04 ± 0.02	96	1300	4.2	90	0.07	1
DC15-22 10m	73.0	11.0	0.47 ± 0.21	0.32 ± 0.14	73	289	23	93	0.25	1
DP11-13 4.3m	28.5	7.0	0.30 ± 0.15	0.82 ± 0.41	29	184	23	150	0.15	1
DP11-13 5.2m	25.0	7.8	0.34 ± 0.13	0.91 ± 0.35	25	160	23	146	0.16	1
DP11-13 7m	72.3	12.0	0.27 ± 0.13	0.62 ± 0.30	72	244	45	150	0.30	1
DP11-13 7.9m	70.8	9.1	0.17 ± 0.09	0.76 ± 0.40	71	199	54	150	0.36	1
DP11-13 8.8m	81.7	11.0	0.32 ± 0.15	0.89 ± 0.42	82	323	39	150	0.25	1
<b>CFO4</b>										
BC4	163.1	35.1	0.37 ± 0.13	0.58 ± 0.20	163	258	95	150	0.63	1
BMW2	595.6	16.5	0.13 ± 0.06	0.21 ± 0.10	596	707	127	150	0.84	1
BMW5	131.2	12.9	0.34 ± 0.16	0.29 ± 0.14	131	520	38	150	0.25	1
BMW6	156.0	0.4	0.01 ± 0.01	0.26 ± 0.26	156	1300	0.4	150	0.12	1
BMW7	134.7	11.6	0.21 ± 0.11	0.41 ± 0.22	135	365	55	150	0.37	1

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