



1 Flexible vector-based spatial configurations in land models

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11 **Abstract.** Land models are increasingly used in terrestrial hydrology due to their process-
12 oriented representation of water and energy fluxes. Land models can be set up at a range of
13 spatial configurations, often ranging from grid sizes of 0.02 to 2 degrees (approximately 2 to 200
14 km) and applied at sub-daily temporal resolutions for simulation of energy fluxes. A priori
15 specification of the grid size of the land models typically is derived from forcing resolutions,
16 modeling objectives, available geo-spatial data and computational resources. Typically, the
17 choice of model configuration and grid size is based on modeling convenience and is rarely
18 examined for adequate physical representation in the context of modeling. The variability of the
19 inputs and parameters, forcings, soil types, and vegetation covers, are masked or aggregated
20 based on the a priori chosen grid size. In this study, we propose an alternative to directly set up a
21 land model based on the concept of Group Response Unit (GRU). Each GRU is a unique
22 combination of land cover, soil type, and other desired geographical features that has
23 hydrological significance, such as elevation zone, slope, and aspect. Computational units are
24 defined as GRUs that are forced at a specific forcing resolution; therefore, each computational
25 unit has a unique combination of specific geo-spatial data and forcings. We set up the Variable
26 Infiltration Capacity (VIC) model, based on the GRU concept (VIC-GRU). Utilizing this model
27 setup and its advantages we try to answer the following questions: (1) how well a model
28 configuration simulates an output variable, such as streamflow, for range of computational units,



29 (2) how well a model configuration with fewer computational units, coarser forcing resolution
30 and less geo-spatial information, reproduces a model set up with more computational units, finer
31 forcing resolution and more geo-spatial information, and finally (3) how uncertain the model
32 structure and parameters are for the land model. Our results, although case dependent, show that
33 the models may similarly reproduce output with a lower number of computational units in the
34 context of modeling (streamflow for example). Our results also show that a model configuration
35 with a lower number of computational units may reproduce the simulations from a model
36 configuration with more computational units. Similarly, this can assist faster parameter
37 identification and model diagnostic suites, such as sensitivity and uncertainty, on a less
38 computationally expensive model setup. Finally, we encourage the land model community to
39 adopt flexible approaches that will provide a better understanding of accuracy-performance
40 tradeoff in land models.

41 **1 Introduction**

42 Land models have evolved considerably over the past few decades. Initially, land models (or land-
43 surface models) were developed to provide the lower boundary conditions for atmospheric models
44 (Manabe, 1969). Since then land models have increased in complexity, and they now include a
45 variety of hydrological, biogeophysical, and biogeochemical processes (Pitman, 2003). Including
46 this broad suite of terrestrial processes makes land models suitable to simulate energy and water
47 fluxes and carbon and nitrogen cycles.

48 Despite the recent advancements in process representation in land models, there is currently
49 limited understanding of the appropriate spatial complexity that is justified based on the available
50 data and the purpose of the modelling exercise (Hrachowitz and Clark, 2017). The increase of
51 computational power, along with the existence of more accurate digital elevation models and land
52 cover maps, encourage modellers to configure their models at the finest spatial resolution possible.
53 Such hyper-resolution implementation of land models (Wood et al., 2011) can provide detailed
54 simulations at spatial scales as small as 1-km² grid over large geographical domains (e.g., Maxwell
55 et al., 2015). However, the computational expense for hyper-resolution models could potentially
56 be reduced using more creative spatial discretization strategies (Clark et al., 2017).



57 It is common to adopt concepts of hydrological similarity to reduce computational costs. In this
58 approach, spatial units are defined based on similarity in geospatial data, under the assumption that
59 processes, and therefore parameters, are similar for areas within a spatial unit (e.g., Vivoni et al.,
60 2004). Hydrological Response Units (HRUs) are perhaps the most well-known technique to group
61 geospatial attributes in hydrological models. HRUs can be built based on various geospatial
62 characteristics; for example, Kirkby and Weyman 1974, Knudsen and Refsgaard (1986), Flügel
63 (1995), Winter (2001), and Savenije (2010) all have proposed to use geospatial indices to discretize
64 a catchment into hydrological units with distinct hydrological behaviour. HRUs can be built based
65 on soil type such as proposed by Kim and van de Giessen (2004). HRUs can also be built based
66 on fieldwork and expert knowledge (Naef et al., 2002, Uhlenbrook 2001), although the spatial
67 domain of such classification will be limited to the catchment of interest and the spatial extent of
68 the field measurements. HRUs are often constructed by GIS-based overlaying of various maps of
69 different characteristics and can have various shapes such as for non-regular (sub-basins), grid,
70 hexagon, or triangulated irregular network also known as TIN (Beven 2001, Marsh et al., 2012,
71 Oliviera et al., 2006, Pietroniro et al., 2007). Similar approaches are used in land models.
72 Traditionally land models use the tiling scheme where a grid box is subdivided into several tiles
73 of unique land cover, each described as a percentage of the grid (Koster and Suarez, 1992). Land
74 models are also beginning to adopt concepts of hydrological similarity (e.g., Newman et al., 2014;
75 Chaney et al., 2018).

76 A long-standing challenge is understanding the impact of grid size on model simulations (Wood
77 et al., 1988). The effect of model grid size can have a significant impact on model simulation
78 across scale especially if the model parameters are linked to characteristics which are averaged out
79 across scale (Bloschl et al., 1995). Shrestha et al. (2015) have investigated the performance of
80 CLM v4.0 coupled with ParFlow across various grid sizes. They concluded the grid size changes
81 of more than 100 meters can significantly affect the sensible heat and latent heat fluxes as well as
82 soil moisture. Also using CLM, Singh et al. (2015) demonstrated that topography has a substantial
83 impact on model simulations at the hillslope scale (~100 meters), as aggregating the topographical
84 data changes the runoff generation mechanisms. This is understandable as the CLM is based on
85 topographical wetness index (Beven and Kirkby 1979, Niu et al., 2005). However, Melsen et al.
86 (2016) evaluated the transferability of parameters sets across the temporal and spatial resolutions
87 for the Variable Infiltration Capacity (VIC) model implemented in an Alpine region. They



88 concluded that parameter sets are more transferable across various grid sizes in comparison with
89 parameter transferability across different temporal resolutions. Haddeland et al. (2002) showed
90 that the transpiration from the VIC model highly depends on grid resolution. It remains debatable
91 how model parameters and performance can vary across various grid resolutions (Liang et al.,
92 2004; Troy et al., 2008; Samaniego et al., 2017).

93 The representation of spatial heterogeneity is an ongoing debate in the land modelling community
94 (Clark et al., 2015). The key issue is to define which processes are represented explicitly and which
95 processes are parameterized. The effect of spatial scale on emergent behaviour has been studied
96 for catchment scale models – the concepts of Representative Elementary Areas (REA), or
97 Representative Elementary Watersheds (REW), were introduced to study the effect of spatial
98 aggregation on system-scale emergent behaviour (Wood et al., 1995, Reggiani et al., 1999). The
99 effect of scale on model simulations is not well explored for land models. More work is needed to
100 understand the extent to which the heterogeneity of process representations is sufficient for the
101 purpose of a given modelling application, and the extent to which the existing data can support the
102 model configurations (Wood et al., 2011, Beven et al., 2015).

103 In addition to the choice on model's spatial configurations, more work is needed to define the
104 appropriate structure of land models. While many studies in hydrology have evaluated how model
105 structure affects the smaller scale watershed response (Son and Sivapalan 2007, Clark et al., 2008,
106 Fenicia et al., 2011, Shafii et al., 2017), this issue has received limited attention in the land
107 modelling community (Desborough, 1999). Only recently, a few land models enable changing the
108 process formulations within a limited range of model structural assumptions (Noah-MP, Niu et al.,
109 2011, SUMMA, Clark et al., 2015) We explore effects of different choices of runoff generation
110 process representation in the model.

111 In this study, we configure the Variable Infiltration Capacity (VIC) model in a flexible vector-
112 based framework to understand how model simulations depend on the spatial configuration. The
113 remainder of this paper is organized as follows: In Section 2, we present the VIC model, its vector-
114 based implementation, and its coupling to the mizuRoute routing model. In Section 3 we describe
115 the design of the experiments. In Section 4 we describe the results of the experiments. Section 5



116 discusses the implication of spatial discretization strategies on large-scale land model applications.
117 The paper ends in Section 6 with conclusions of this study and implications for future work.

118 **2 Land model and the routing model**

119 *2.1 The Variable Infiltration Capacity (VIC) model*

120 The VIC model was developed as a simple land surface/hydrological model (Liang et al. 1994)
121 that has received applications worldwide (Melsen et al., 2016). In this study we use classic VIC
122 version 5 (VIC-5, Hamman et al., 2018). The key features of VIC are: (i) traditionally, the VIC
123 model (version 4 and earlier) simulates sub-daily energy variables with daily forcing of minimum
124 and maximum temperature, precipitation and wind speed. This enables the VIC model to be easily
125 forced with hydrological available data sets worldwide while being able to solve the energy fluxes
126 over sub-daily time periods. (ii) The VIC model combines sub-grid probability distributions to
127 simulate surface hydrology such as variable infiltration capacity formulation (Zhao, 1982) with
128 bio-physical formulations for transpiration (Jarvis et al., 1976).

129 The VIC model uses three soil layers to represent the subsurface. While each soil layer can have
130 various physical soil parameters (e.g., saturated hydraulic conductivity, bulk density), each layer
131 is assumed to be uniform across the entire grid regardless of the vegetation type variability in that
132 grid. The VIC model assumes a tile vegetation implementation within each grid similar to the
133 mosaic approach of Koster and Suarez (1992). To account for spatial variability in vegetation, the
134 VIC model allows for root depths to be adjusted for every vegetation type. The vegetation
135 parameters (e.g., stomatal resistance, LAI, albedo) are fixed for every land cover. The VIC model
136 can account for different elevation zones to account for temperature lapse rate given elevation
137 difference in a grid cell, and also for the distribution of precipitation over various elevation zones.

138 *2.2 The VIC-GRU implementation: a vector-based configuration for land models*

139 The VIC model is typically applied at regular grid. Figure-1a illustrates the typical VIC
140 configuration – here the modeler selects a cell size, and then the soil, vegetation and forcing files
141 are all aggregated or disaggregated to the target cell size. Original data resolution and spatial
142 distribution of soil, land cover and forcing data are lost. In this study, we configure the VIC model



143 using non-regular shapes, Grouped response Units (GRUs, Kouwen et al., 1993), depending on
144 the soil, vegetation, and topography. The GRUs hence describe unique characteristics of soil,
145 vegetation type, elevation, slope and aspect. Figure-1b presents an example of irregular GRUs
146 created through spatial intersections of the land use and soil types. These GRUs then can be forced
147 at the original resolution of forcing, or upscaled or downscaled values. Computational units can
148 then be constructed that intersect the GRUs with the forcing grid. Therefore, each computational
149 unit has unique geospatial data such as soil, vegetation, slope and aspect and is forced with a unique
150 forcing (a specific GRU forced with unique forcing).

151 The benefits of vector-based implementation of the VIC model based on the concept of GRU can
152 be summarized as follows:

153 **1- No grid and no assumption on grid size; Model resolution loses its meaning.** In
154 traditional VIC implementation, the modeler selects a grid resolution (which is often a regular
155 latitude/longitude grid). The soil parameters and forcing data from any resolution must be
156 aggregated, disaggregated, resampled or interpolated for every grid size. The land cover data is
157 only considered as a percentage for every grid and spatial location of the land cover is lost.
158 However in the VIC-GRU setup these decisions are only based on the input and forcing data that
159 are chosen to be used in the modeling practice and no upscaling or downscaling to grid size is
160 needed.

161 **2- The GRUs at the resolution of the forcing data logically represent the heterogeneity**
162 **of the input data (meteorological forcing and geospatial information).** A higher number of
163 computational units than the proposed setup will arguably provide an unnecessary computational
164 burden due to identical forcing data and geospatial information.

165 **3- Direct simplification of geospatial data.** The vector-based implementation makes the
166 direct aggregation of GRUs based on merging the geospatial data. It is easier to aggregate similar
167 soil types or similar forested areas into a unified GRU with basic GIS function (dissolving for
168 example) than this would be if all data had to be converted to a uniform grid first.

169 **4- Direct specification of physical parameters.** As each of the GRUs have specific type of
170 land cover, soil type and other physical characteristics, it is straightforward to specify parameter



171 values based on look up tables (i.e., no averaging, upscaling or smearing is needed). This is
172 favorable because the modeler does not need to make decisions about methods used for upscaling
173 of geophysical data at the grid level.

174 **5- The ability to compare and constrain the parameter values for GRUs and their**
175 **simulations.** The impact of land cover, soil type and elevation zone can be evaluated separately.
176 For example, the GRU concept makes it easier to test if forested areas generate less surface runoff
177 than grasslands. The new implementation of VIC simplifies using knowledge of geospatial
178 properties (e.g., soils data) and hydrological processes (e.g., expected fluxes for specific GRUs) to
179 constrain model parameter values. Similarly, the GRU concepts simplify regularization across
180 large geographical domains.

181 **6- Avoid unrealistic combinations of land cover, soil and elevation zone.** Unlike the
182 traditional VIC configuration, the proposed VIV-GRU approach avoids unrealistic configuration
183 of land cover, soil and elevation zones. An example is presented in Figure-2. This setup is with
184 two elevation zones partitioned at the tree line and two land cover types, forest below tree line and
185 bare soil above the tree line. The traditional VIC configuration assumes four different
186 combinations, including the unrealistic case of forest above the tree line. This issue is avoided in
187 vector-based setup of VIC-GRU as the set up will only include two GRUs with forest for lower
188 elevation and with bare soil for higher elevation.

189 **7- Possibility to incorporate additional data.** If needed, additional data such as slope and
190 aspect can be incorporated into the GRUs, accounting for changes in shortwave radiation or lapse
191 rates for temperature. These additional controls can be implemented outside of the model in the
192 forcing files. GRUs can be built also based on variation of leaf area index (LAI) giving an
193 additional layer of information in addition to the land cover type.

194 **8- Easier comparison of model simulations and in situ point-scale observation and**
195 **visualization:** The GRU implementation makes it easier to compare the point measurement to
196 model simulation as the model simulations preserve extent of geospatial features. The GRU
197 implementation also simplifies the comparison across GRUs; this comparison is very difficult in
198 the typical VIC implementation because of the need to upscale geophysical information to the grid
199 scale.



200 **9- Modular and controlled selection of models:** The GRU implementation identifies the
201 characteristics and spatial boundary of geospatial domains. A model might not be suitable for
202 processes of some of the geospatial domains. Alternatively, processes of a GRU that is beyond the
203 capacity of one model can be replaced with an alternative model. For example glaciers, can be
204 replaced with more suitable models while the configuration and forcings remain identical.
205 Consequently, the effect of features such as glacier can be better studied at larger scale
206 hydrological cycle as more expert models can be applied to glacier while the rest of the GRUs can
207 be simulated with a model that includes general processes.

208 2.3 *Structural changes in VIC-GRU*

209 We implemented several changes to the VIC process equations:

210 1- The VIC model uses the ARNO formulation, or its Nijssen representation, to represent
211 baseflow (Todini et al., 1996, Nijssen et al., 2001). In this study we simplify the VIC baseflow
212 formulation to a linear reservoir with one parameter, K_{slow} .

213 2- Preferential flow pathways are added to the VIC model by partitioning the runoff (fast
214 reacting component of the VIC model) into (1) an effective surface flow component; and (2)
215 recharge to the baseflow reservoir (interpreted as macropore flow). This partitioning is
216 parameterized based on the macropore fraction (for further reading on the implementation refer to
217 Gharari et al., 2019).

218 3- It is assumed that vegetation roots are restricted to the first two layers of the soil. This is
219 due to the simplification of the VIC baseflow formulation.

220 2.4 *mizuRoute, a vector-based routing scheme*

221 In this study, we use the vector-based routing model mizuRoute (Mizukami et al., 2016). Vector-
222 based routing models can be configured for separate computational units than the land model (e.g.,
223 configuring routing models using sub-basins derived from existing hydrologically conditioned
224 DEMs such as Hydrosheds, Lehner et al., 2006, or Merit Hydro, Yamazaki et al., 2019). This
225 removes the dependency of the routing to the grid size or GRUs configurations, and eliminates the
226 decisions that are often made to represent routing-related parameters at grid scale. Therefore we



227 can ensure that two model configurations with different geospatial configurations are routed using
228 the same routing configuration. The intersection between the computational units in the land model
229 and the sub-basins in the routing model defines the contribution of each computational units in the
230 land model to each river segment.

231 **3 Data and methods**

232 *3.1 Experimental design*

233 In this study, we configure the VIC model in a flexible vector-based framework to understand how
234 model simulations depend on the spatial configuration. We consider four different methods to
235 discretize the landscape for seven different spatial forcing grids (see Table 1). The landscape
236 discretization methods include (1) simplified land cover and soils; (2) full detail for land cover and
237 soils; (3) full detail for land cover and soils, including elevation zones; and (4) full detail for land
238 cover and soils, including elevation zones and slope and aspect. The different spatial forcing grids
239 are 4-km, 0.0625°, 0.125°, 0.25°, 0.5°, 1°, and 2°. This design enables us to separate our method to
240 discretize the landscape from the spatial resolution of the forcing data.

241 Experiments are performed for the Bow River at Banff with a basin area of approximately 2210
242 km². The Bow River is located in the Canadian Rockies in the headwaters of the Saskatchewan
243 River Basin. Most of the Bow River streamflow is due to snow melt (Nivo-glacial regime). The
244 average basin elevation is 2130 m ranging from 3420 m at the peak top to 1380 m above mean sea
245 level at the outlet (town of Banff). The basin annual precipitation is approximately 1000 mm with
246 range of 500 mm for the Bow Valley up to 2000 mm for the mountain peaks. The predominant
247 land cover is conifer forest in the Bow Valley and bare soil and rocks for mountain peaks above
248 the tree line.

249 We design three experiments:

250 3.1.1 Experiment-1: How does the spatial configuration affect model performance?

251 As the first experiment, we focus on how well the various configurations simulate observed
252 streamflow at the Bow River at Banff. We calibrate the parameters for the different configurations
253 in Table 1. Model calibration is accomplished using the Genetic Algorithm implemented in the



254 OSTRCIH framework (Mattot, 2005; Yoon and Shoemaker, 2001), maximizing the Nash-Sutcliffe
255 Efficiency (ENS , Nash and Sutcliffe 1970) using a total budget of 1000 model evaluations given
256 the available resources limited by the most computationally expensive model (Case-4-4km).

257 3.1.2 Experiment-2: How well do calibrated parameter sets transfer across different model
258 configurations?

259 As the second experiment, we focus on how various configurations can reproduce the result from
260 the configuration with highest computational units for a given parameter set. In other words, this
261 experiment evaluates accuracy-efficiency tradeoffs – i.e., the extent to which spatial
262 simplifications affect model performance under the assumption that similar GRUs possess
263 identical parameters across various configurations. This is important as it enables modelers to
264 understand efficiency-accuracy tradeoffs, given the available data and the purpose of the modelling
265 application. This experiment is based on perfect model experiments using the model with the
266 highest computational unit as synthetic case (Case-4-4km). Synthetic streamflow for every river
267 segment is generated using a calibrated parameter set for Case-4-4km-4km. The models with lower
268 number of computational units are then simulated using the exact same parameter set used for
269 generating the synthetic streamflow. The differences in streamflow simulation, quantified using
270 ENS , provide an understanding of how the simulations deteriorate when the spatial and forcing
271 heterogeneities are masked or up-scaled. This also will bring an understanding on how sensitive
272 the changes are along the river network and at the gauge location at which the models are calibrated
273 against the observed streamflow data. Similarly, we compare the spatial patterns of snow water
274 equivalent for the different spatial configurations.

275 3.1.3 Experiment 3: How do different model structures affect model performance?

276 As the third experiment, we focus on the effect of model structure on the performance metric (ENS).
277 This experiment, although not directly linked to the exploration of spatial configuration, is
278 designed to investigate the effect of model structure changes on model performance which may
279 affect our perception of parameter allocation across the GRUs (non-uniqueness of models,
280 processes and parameter values)... For Case-2-4km, we calibrate the model with macropores
281 activated and micropore deactivated. We call this model Case-2-4km-macro. We compare the



282 general model behavior looking into surface runoff and base-flow proportions of the streamflow
283 for GRUs for the two model setups, Case-2-4km and Case-2-4km-macro.

284 3.2 Geospatial data and meteorological forcing

285 The inputs and forcing we used to set up the models are as follows:

286 1- Land cover: We used the land cover map NALCM-2005 v2 that is produced by CEC
287 (Latifovic et al., 2004). NALCM-2005 v2 includes 19 different classes. The land cover map is used
288 to set up the vegetation file and vegetation library (look up table) for the VIC model (Nijssen et
289 al., 2001).

290 2- Soil texture: We used the Harmonized World Soil Data, HWSD (Fischer et al., 2008). For
291 each polygon of the world harmonized soil we use the highest proportion of soil type. The HWSD
292 provide the information for two soil layers, in this study we base our analyses on the lower soil
293 layer reported in HWSD to define the soil characteristics needed for the VIC soil file.

294 3- Digital Elevation Model: in this study we make use of existing hydrologically conditioned
295 digital elevation models to (1) derive the river network topology for the vector-based routing,
296 mizuRoute and (2) to derive the slope, aspect and elevation zones which are used to estimate the
297 forcing variables. For the first purpose we use hydrologically condition DEM of HydroSHED with
298 resolution of 3 arc-second, approximately 90 meters; for the second purpose we use HydroSHED
299 15 arc-second DEM (approximately 500 meters).

300 4- Meteorological forcing: we used the WRF data set with the temporal resolution of 1 hour
301 and spatial resolution of 4 km (Rasmussen and Liu, 2017). For upscaling the WRF input forcing,
302 we use the CANDEX package (DOI: 10.5281/zenodo.2628351) to map the 7 forcing variables to
303 various resolutions (1/16°, 1/8°, 1/4°, 1/2°, 1° and 2° from the original resolution of 4 km). We used
304 the required variables from the WRF data set namely, total precipitation, temperature, short and
305 long wave radiation at the ground surface, V, U components of wind speed and water vapor mixing
306 ratio.

307 The shortwave radiation is rescaled based on the slope and aspect of the respective GRUs (refer to
308 Appendix-A for more details). In this study we differentiated four aspects and five slope classes.



309 The temperature at 2 meters are adjusted using the environmental lapse rate for temperature of 6.5
310 km per 1000 meters. The assumed lapse rate aligns with earlier findings from the region of study
311 (Pigeon and Jiskoot, 2008).

312 3.3 *Observed data for model calibration*

313 The daily streamflow is extracted from the HYDAT (WSC, Water Survey Canada) for Bow at
314 Banff with gauges ID of 05BB001. This data is used for parameter calibration/identification of
315 VIC-GRU parameter values.

316 3.4 *Model parameters*

317 3.4.1 VIC-GRU parameters

318 In the experiments for this study, we calibrate a subset of VIC parameters namely b_{inf} , E_{exp} , K_{sat} ,
319 $d_{2,forested}$, $d_{2,non-forested}$ and K_{slow} and $D_{macro-fract}$ (names are mentioned in Table-2). We make sure that
320 the $d_{2,forested}$ is larger than the $d_{2,non-forested}$ as the root depth are deeper for forested regions
321 (constraining relative parameters).

322 3.4.2 MizuRoute parameters:

323 Impulse Response Function (IRF) routing method (Mizukami et al., 2016) is used for this study.
324 IRF, which is derived based on diffusive wave equation, includes two parameters – wave velocity
325 and diffusivity. The parameters for the routing scheme and river network topology for the
326 mizuRoute is identical for all the configurations and experiments. The river network topology,
327 assuming 100 km² starting threshold for the sub-basin size, is based on a 92-segment river network
328 depicted in Figure-3d. The diffusive wave parameters are set to 1 m/s and 1000 m²/s respectively
329 and remain identical for all the river segments.

330 4 **Results**

331 4.1 *Experiment-1*

332 The various model configurations are compared with respect to the Nash-Sutcliffe performance
333 metric (E_{NS}). Results show that all the models, including the ones that are configured with coarser



334 resolution forcings, can simulate streamflow with E_{NS} as high as 0.70 (Table-3). These results
335 indicate that the coarse resolution forcing input and lower computational units are able to yield
336 equivalent E_{NS} of 0.7 and higher.

337 Although the performance metric of the various configurations, it is noteworthy to mention that
338 the configuration of Case-4-0.5° has higher E_{NS} value compared to the cases with highest
339 computational units, Case-4-4km for example. This might be due to various reasons including: (1)
340 compensation of forcing aggregation on possible forcing bias at finer resolution; (2) compensation
341 of forcing aggregation on model states and fluxes and possible adjustment for model structural
342 inadequacy and hence directing the optimization algorithm to different possible solutions across
343 configurations.

344 The model simulations, with E_{NS} higher than 0.7 for example, have very different soil parameters
345 configuration. As an example, saturated hydraulic conductivity, K_{sat} , and slope of water retention
346 curve, E_{exp} , can have very different combinations of values within the specified ranges for the
347 parameters. Figure-4 illustrates the possible combinations of K_{sat} and E_{exp} with performance higher
348 than E_{NS} greater than 0.7 for Case-2-4km. The result indicates the two parameters that are often
349 fixed or a priori allocated based on look up tables can exhibit significant uncertainty and non-
350 identifiability. Moreover, calibrating the VIC model using a sum-of-squared objective function at
351 the basin outlet does not constrain the VIC soil parameters.

352 4.2 Experiment-2

353 The second experiment compares the performance of a parameter set with E_{NS} of above 0.7 from
354 the Case-4-4km across the configurations with degraded geophysical information and aggregated
355 spatial information. Figure-5 shows the evaluation metric, E_{NS} , for the streamflow of every river
356 segment across the domain in comparison with the synthetic case (Case-4-4km). From Figure-5,
357 it is clear that the E_{NS} is less sensitive for river segments with larger upstream area (read more
358 downstream). This result has two major interpretations (i) the parameter transferability across
359 various configuration is dependent on the sensitivity of simulation at the scale of interest and (ii)
360 often inferred parameters at larger scale may not guarantee good performing parameters at the
361 smaller scales.



362 Figure-6 shows the performance of the streamflow across various configurations for the most
363 downstream river segment (the gauged river segment which is often used for parameter inference
364 through calibration). Figure 6 illustrates that most of the configurations have similar scaled E_{NS} at
365 the basin outlet. This analysis can be repeated for different parameter sets, e.g., poorly performing
366 parameter sets or randomly selected parameter sets, to better understand accuracy-efficiency
367 tradeoffs. Such analyses can provide insights on the appropriate model configurations for different
368 applications. As an example, if model configurations of different complexity are known to show
369 similar performance for a given parameter set, uncertainty and sensitivity analysis can be done
370 initially on the models with fewer computational units and the results of the analysis can be applied
371 to models with a higher number of computational units. This is however under assumption that
372 parameters are transferable based on the concept of GRU.

373 To understand the spatial patterns of model simulations for all the configurations, we evaluate the
374 distribution of the snow water equivalent, SWE, for the computational units on 5th of May 2004
375 (Figure-7). In general, the SWE follows the forcing resolution and its aggregation. Although
376 coarser forcing resolutions results in coarser SWE simulation, the geospatial details such as
377 elevation zones and slope and aspects result in more realistic representation of SWE as the snow
378 layer is thinner for south facing slopes where more melt can be expected to occur, and thicker for
379 higher elevation zones (compare SWE simulations for Case-4-2° and Case-3-2° in Figure-7) which
380 is consistent with higher precipitation volumes and slower melt at higher elevation. Another
381 observation from Figure-7 is the unrealistic distribution of SWE for configurations without
382 elevation zones (Case-2 and Case-1). The lack of elevation zones results in both valley bottom and
383 mountain tops to be forced with the same temperature. Snow is more durable in the forested areas
384 as the result of model formulation, which are at lower elevation, while SWE is less for higher
385 mountains, which is unrealistic.

386 We compared the maximum snow water equivalent across different configurations for a
387 computational unit located in the Bow Valley Bottom (an arbitrary location of -116.134°W and
388 51.382°E) for the year 2004. Figure-8 illustrated the maximum snow water equivalent for the
389 period of simulation. The result indicates that the SWE is higher for configurations with coarser
390 forcing resolutions (almost double). This is due to the reduced temperature as a result of masking
391 warmer valley bottom by cooler and higher forcing grids over the Rockies.



392 4.3 Experiment-3

393 The calibration of model Case-2-4km and Case-2-4km-macro result in similar E_{NS} values of 0.78
394 and 0.75, indicating that both models are able to reproduce the observed streamflow to a similar
395 extent although they are structurally different (the slow reservoir is recharged through only
396 micropore and only macropore water movement in Case-2-4km and Case-2-4km-macro
397 respectively). Figure-9 shows the streamflow hydrographs for the best performing parameter sets.
398 . Observed Bow River at Banff has a minimum streamflow of approximately 15 cubic meter per
399 second during snow accumulation months. This flow may be the result of regulation, return flow
400 from human activities or unaccounted processes such as groundwater flow which are rather
401 difficult for the linear reservoir of baseflow to simulate. Results (not shown) also indicate that both
402 models structures generate 4 to 5 times more baseflow than surface runoff. This might be very
403 intuitive as the model structure and parameters only have one processes, the slow reacting
404 component, to simulate the long memory of this Nivo-glacial system and its annual cycle. Even
405 though the two models are structurally different, both produce flow volumes through the surface
406 and baseflow pathways that are consistent with streamflow observation. Similar to the uncertainty
407 of model parameters, this result also shows the uncertainty of model structure and the fact that
408 inclusion or exclusion of macropore water movement in the region of study and the context of
409 modeling, may not change the overall results and similarly that these processes, micropore or
410 macropore flow, cannot be inferred from the streamflow observation only.

411 5 Discussion

412 In this study, we proposed a vector-based configuration for land models and applied this setup to
413 the VIC model. We used a vector-based routing scheme, mizuRoute, which was forced using
414 output from the land model (one-way coupling). We term this new modelling approach VIC-GRU.
415 Unlike the grid-based approach, there is no upscaling of land cover percentage or soil
416 characteristics to a new grid size. This enables us to separate the effects of changes in forcing from
417 changes in the spatial configurations. The vector-based setup also provides us with more flexibility
418 in comparing the model simulations across GRUs, and also comparing model simulations with
419 point measurements, such as snow water equivalent.



420 Our results illustrate that the VIC-GRU approach generates similar large-scale simulations of
421 streamflow across the various spatial configurations when VIC-GRU is calibrated by maximizing
422 the Nash-Sutcliffe score at the basin outlet. Similarly, we have shown that the VIC soil parameters
423 can be very different when calibrated using different spatial configurations and that parameter
424 transferability to different forcing resolutions and model setups is limited. This uncertainty is not
425 often evaluated or reported for land models (Demaria et al., 2007) or is ignored by tying
426 parameters, linking specific hydraulic conductivity to the slope of water retention curve, for
427 example, so that the possible combination of them are reduced.

428 Land models are often applied at large spatial scales. The results clearly show that the deviation
429 of streamflow is much lower in river segments with larger upstream area (Figure 5 and 6). It is
430 often the case that the model parameters are inferred based on calibration on the streamflow at the
431 basin outlet or over a large contributing area. We argue that this may not be a valid strategy for
432 process understanding at the GRU scale, given the large uncertainty exhibited by the parameters.
433 Therefore, hyper-resolution modeling efforts, Wood et al. 2011, may suffer from poor process
434 representation and parameter identification at the scale of interest (Beven et al., 2015). What is
435 needed instead of efficiency metrics that aggregate model behavior across both space (e.g. at the
436 outlet of the larger catchment) and time (e.g. expressing the mismatch between observations and
437 simulations across the entire observation period as a single number), is diagnostic evaluation of
438 the model's process fidelity at the scale at which simulations are generated (e.g. Gupta et al., 2008;
439 Clark et al., 2016).

440 We have shown that changes in model structure can result in identical performance for system-
441 scale evaluation metrics (in this case, the Nash Sutcliffe Efficiency). We have changed the land
442 model structure by replacing the micropore with macropore water movement to the slow reservoir.
443 Similar to the parameter uncertainty, this indicates that lack or inclusion of macropore processes
444 at the GRU scale does not have any notable effect on the efficiency score of the model simulation
445 of streamflow at the outlet of the basin, even though the process simulations at the GRUs are
446 different. Alternatively, this also shows that the micropore and macropore processes and their
447 parameters may not be identifiable through calibration on the observed streamflow, which supports
448 the argument against assuming that fine-scale parameters and processes can be inferred from large-
449 scale observations. Although in this study we only focus on the processes and parameters that are



450 often used to calibrate for the VIC model such as subsurface processes, it is possible to repeat the
451 same analysis on wider range of processes such as snow processes or routing parameters.

452 It is often computationally expensive to evaluate the uncertainty and sensitivity of land models.
453 Following the results presented in Figure-6, one can assume a configuration with fewer
454 computational units can be a surrogate for a model with more computational units, under the
455 condition that both models are known to behave similarly for a given parameter set. The calibration
456 can be done on the model configuration with less computational unit and the parameters can be
457 transferred directly to the model with more computational units, or can be used as an initial point
458 for optimization algorithm to speed up the calibration process. Similarly the sensitivity analyses
459 can be done primarily on the model with less computational units.

460 One might argue that the spatial discretization is important for realism of model fluxes and states.
461 Moving to significantly high number of GRUs may result in computational units that are similar
462 in their forcing and spatial variability. Based on the result of this study for snow water equivalent
463 (Figure-8), we can argue that the snow patterns are fairly similar for the configurations that have
464 elevation zones and finer resolution of forcing (case3 and 4 and forcing resolution less than 0.125
465 degree). It can be further explored if the model simulation at finer resolutions can be approximated
466 by interpolating result of a model with coarser resolution ($m(\bar{x}|\theta) \sim \overline{m(x|\theta)}$, in which m is the
467 model, x is forcing and θ is the parameter set).

468 In this study and following the concept of GRUs, Grouped Response Units, we assumed the
469 physical characteristics of soil and vegetation are identical for a given GRU across various model
470 configurations. Techniques such as multiscale parameter regionalization (MPR, Samaniego et al.,
471 2010) can be used to scale parameter values for different model configurations. However, applying
472 these techniques, such as in this case that has significant parameter and process uncertainty and
473 significance accuracy-performance tradeoff, should be put through rigorous tests (Merz et al.,
474 2020, Liu et al., 2016).

475 Also, the degree of validity of the concept of GRU, hydrological similarity based on physical
476 attribute similarities, is debatable. For example, at the catchment scale, Oudin et al. (2010) have
477 shown that the overlap between catchments with similar physiographic attributes and catchments
478 with similar model performance for a given parameter set is only 60%. Physiographic similarity



479 (in our case expressed through GRUs) does thus not necessarily imply similarity of hydrologic
480 behavior, even though this is the critical assumption underlying GRUs. Although the GRUs in this
481 study include slope and aspect, these characteristics were not translated into the model parameters
482 and was only used for forcing manipulation. The VIC parameters can be linked to many more
483 characteristics such as slope, height above nearest drainage (HAND, Renno et al., 2008), or
484 Topographical Wetness Index (Beven and Kirkby, 1979) as has been done by Mizukami et al.
485 (2017) and Cheney et al. (2018). However the functions that are used to linked the attribute to
486 model characteristics remains mostly assumptions rather than inference and reproducibility of
487 them are not very well explored (if possible).

488 In this study, the vector-based routing configuration does not include lakes and reservoirs. This is
489 often a neglected element of land modeling efforts and has only attracted limited attention
490 compared to the its impact on terrestrial water cycle (Haddeland et al., 2006, Yassin et al., 2018).
491 The presence of lakes and reservoirs and their interconnections reduces the, already limited, ability
492 of inference of land model parameter based on calibration on the observed streamflow because
493 streamflow variability is reduced.

494 Although not primary the result of this study, however, the Nivo-glacial regime of the Bow River
495 Basins is mostly dominated by snow melt that contributes to streamflow through baseflow (slow
496 component of the hydrograph). The high Nash-Sutcliffe Efficiency, E_{NS} , is partly due to the fact
497 that it is rather easy for the land model to capture the yearly cycle of the streamflow only with
498 snow processes while rapid subsurface water movement, such as macropore, are largely missing
499 in the land models but do not lead to notably increased efficiency scores when they are included
500 in the model structure. More caution is needed for use of the land model for flood forecasting
501 (Vionnet et al., 2019) for this region and all the Nivo-glacial river systems in western Canada,
502 McKenzie, Yukon and Colombia River Basins.

503 **6 Conclusions**

504 The vector-based setup for the land model can provide modelers with more flexibility, e.g. impact
505 of various forcing resolution or geospatial data representation, while avoiding decisions that are
506 often taken for model configuration at grid level. The conclusion and messages from this study
507 can be summarized as follows:



- 508 1) Regardless of observations at the scale of modeling, a model configuration with lower
509 computational units, coarser resolution and less geospatial information, can produce model
510 simulations with similar efficiency scores as configurations with higher computational
511 units. The choice of model set up should be tested within the context and purpose of
512 modeling for every different case.
- 513 2) The model with the highest number of computational units may not result in improved
514 performance and better spatial simulation, in terms of obtained efficiency scores, and
515 parameters can be transferred without substantial performance changes between certain
516 model setups. Less computationally expensive configurations can be used instead for
517 primary uncertainty and sensitivity analysis.
- 518 3) There is significant parameter and structural uncertainty associated with the VIC-GRU
519 model. This uncertainty creates challenges for the process and parameter inference using
520 calibration on streamflow. Any regionalization for parameters of the model should take
521 into account these significant uncertainties. Our results recommend caution and more
522 attention to the topic of parameter and process inference at finer modelling scales.

523 We also encourage the need for tools which can facilitate easier and more flexible set up of land
524 models that in turn can facilitate the above mentioned research questions.

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527 **Data availability.** All the data used in this study are available publicly (refer to references).

528 **7 Appendix**

529 *7.1 Appendix – A*

530 This appendix reflect on the methods and equations that have been used to calculate the ration of
531 the solar radiation to flat surface and a surface with slope and aspect.

532 **Declination angle:** declination angle can be calculated for each day of year and is the same for
533 the entire Earth based on (Ioan Sarbu, Calin Sebarchievici, in Solar Heating and Cooling Systems,
534 2017):



$$535 \quad \delta = 23.45 \frac{\pi}{180} \sin \left[\frac{2\pi}{360} \frac{360}{365} (284 + N) \right] \quad (\text{A-1})$$

536 In which N is the number of day in a year starting from beginning 1st of January.

537 **Hour angle:** is the angle expressed the solar hour. The reference of solar hour angle is solar noon
538 (hour angle is set to zero) when the sun is passing the meridian of the observer or when the solar
539 azimuth is 180. The hour angle can be calculated based on the:

$$540 \quad \sin \omega = \frac{\sin \alpha - \sin \delta \sin \phi}{\cos \delta \cos \phi} \quad (\text{A-2})$$

541 In which α , ϕ and δ are the altitude angle, latitude of the observer and inclination angle.

542 The solar noon is not exactly coinciding with 12 am of the local time zone. However in this study
543 we assume the two property are coinciding. The sunset and sunrise hour can be calculated from:

$$544 \quad \cos \omega_s = -\tan \phi \tan \delta \quad (\text{A-3})$$

545 For beyond 66.55 degree if the value of the right hand side is above 1 then there is 24 hour of
546 daylight and if the right hand side is less than 1 the will be 24 hour of darkness.

547 The number of daylight hours that can be split before and after the solar noon equally can be
548 calculated based on (assuming 15 degree for every 1 hour):

$$549 \quad n = \frac{2\omega_s}{15} \frac{180}{\pi} \quad (\text{A-4})$$

550 **Altitude angle:** is the angle of sun with the observer. This angle is maximum at solar noon and 0
551 for subset and sunrise. The altitude angle can be calculated based on the:

$$552 \quad \sin \alpha = \sin \delta \sin \phi + \cos \delta \cos \omega \cos \phi \quad (\text{A-5})$$

553 For the solar noon when ω , hour angle, is zero the question simplifies to:

$$554 \quad \sin \alpha = \sin \delta \sin \phi + \cos \delta \cos \phi = \cos(\phi - \delta) = \sin \left(\frac{\pi}{2} - \phi + \delta \right) \quad (\text{A-6})$$

555 This result the altitude angle for the solar noon to be:



$$556 \quad \alpha = \frac{\pi}{2} - \phi + \delta \quad (A-7)$$

557 **Solar Azimuth:** The solar azimuth angle, θ_{Sun} reflect on the angle of the sun on the sky from the
558 North with clockwise rule. The azimuth angle can be calculated as:

$$559 \quad \sin \theta_{Sun} = \frac{\sin \omega \cos \delta}{\cos \alpha} \quad (A-8)$$

560 The solar azimuth angle for the solar noon is set to be 180 degree (calculated clockwise from north
561 direction).

562 The azimuth at the sunset and sunrise can be calculated using:

$$563 \quad \sin \theta_{Sun,rise} = -\sin \omega_s \cos \delta \quad (A-9)$$

$$564 \quad \sin \theta_{Sun,set} = \sin \omega_s \cos \delta \quad (A-10)$$

565 **Surface Azimuth (a.k.a. aspect):** The surface azimuth angle, $\theta_{Surface}$ reflect the direction of the
566 any tilted surface to the north direction. This azimuth is fixed for any point while the solar azimuth
567 changes over hours and seasons.

568 **Angle of incidence θ :** this angle represent the angle between a sloped surface and the sun rays
569 that reaches this sloped surface. The model angle of the incidence for a slope surface β , and aspect
570 of $\theta_{Surface}$ over latitude of ϕ can be calculated as (Kalogirou, in Solar Energy Engineering, 2009,
571 in the reference formulation the Azimuth is from south which is corrected here for North):

$$572 \quad \cos \theta = \sin \delta \sin \phi \cos \beta + \sin \delta \cos \phi \sin \beta \cos \theta_{Surface} + \cos \delta \cos \phi \cos \beta \cos \omega - \\ 573 \quad \cos \delta \sin \phi \sin \beta \cos \theta_{Surface} \cos \omega - \cos \delta \sin \beta \sin \theta_{Surface} \sin \omega \quad (A-11)$$

574 For the flat surface, both $\theta_{Surface}$ and β , is set to zero, the incident angle can be calculated for the
575 flat surface as

$$576 \quad \cos \theta_{flat} = \sin \delta \sin \phi + \cos \delta \cos \phi \cos \omega \quad (A-12)$$

577 In case where the angle of incident is larger than 90 degrees the surface shades itself.



578 **Amendment of short wave radiation based on slope and aspect.** In this study we correct the
579 WRF short wave radiation based on the surface slope and aspect. We first back calculated the
580 incoming short wave radiation by dividing the provided short wave radiation by the cosine of the
581 incident angle of the flat surface. Then we can calculate the solar radiation of the sloped surface
582 multiplying this value to the cosine of the incident angle of the slope surface. Basically this ratio
583 is:

$$584 \quad R = \frac{\cos \theta}{\cos \theta_{flat}} \quad (\text{A-13})$$

585 The effect of the atmosphere is considered in the WRF product itself. However, and for incident
586 level close to 90 degrees the ratio, R , might be very high values which result in the surface
587 receiving unrealistically high value of radiation even higher than the solar constant, 1366 W/m²,
588 at the top of the atmosphere. For cases with cos values of incident angle lower than 0.05 we set
589 the ratio to 0 to avoid this unrealistic condition.

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786 **9 Tables**

787 Table – 1 the number of computational units for the Bow River at Banff, given different spatial
 788 discretization of land cover, soil type, elevation zones and slope and aspects forced with various
 789 forcing resolutions.

	Forcing resolution	Case 4 4 aspect groups; 5 slope groups; 19 classes of land cover; 500 meter elevation zones;	Case 3 no aspect groups; no slope groups; 19 classes of land cover; 500 meter elevation zones;	Case 2 no aspect groups; no slope groups; 19 classes of land cover; no elevation zones;	Case 1 no aspect groups; no slope groups, 3 classes of land cover, one dominant soil type no elevation zones;
Number of GRUs	--	582	65	56	3
Number of Computational units (GRUs forced at various forcing resolutions)	4km	6631	1508	941	479
	0.0625	5224	1098	663	290
	0.125	3079	515	283	94
	0.25	2013	306	154	39
	0.5	1332	184	93	21
	1.0	917	116	56	12
	2.0	767	89	42	6

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794 Table-2 the VIC-GRU model parameters that are subjected to perturbation for model calibration
 795 for the designed experiments.

Parameter symbol	Parameter name	Minimum value	Maximum value	Unit	Explanation
b_{inf}	Variable infiltration parameter	0.01	0.50	[-]	
E_{exp}	The slope of water retention curve	3.00	12.00	[-]	
K_{sat}	Saturated hydraulic conductivity	5.00	1000.00	[mm/day]	Fixed at very low rate, 0.0001, for the macropore model in experiment 3 to disable micropore water movement to the slow reservoir.
d_1	The depth of top soil layer	0.2	0.2	m	Fixed at 20 cm for both forested and non-forested GRUs
$d_{2,forested}$	The depth of the second soil layer for forested GRUs	0.2	2	m	
$d_{2,non-forested}$	The depth of the second soil layer for non-forested GRUs	0.2	$d_{2,forested}$	m	The maximum is bounded by the $d_{2,forested}$
D_{root}	The distribution of root in the two soil layers.	0.5	0.5		Fixed at 50% for the top and lower soil layers.
K_{slow}	Slow reservoir coefficient	0.001	0.9	[1/day]	
$D_{macro-fract}$	Macropore fraction	0.0	1.0	[-]	Fixed at 0.00 for experiment 1 and experiment 2, varying for experiment 3.

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801 Table-3 – The E_{NS} for the different model configurations. Details on the geospatial cases are
802 provided in Table 1.

Forcing resolution	Case 4	Case 3	Case 2	Case 1
4km	0.80	0.80	0.78	0.74
0.0625°	0.80	0.80	0.78	0.77
0.125°	0.80	0.80	0.76	0.73
0.25°	0.82	0.81	0.76	0.76
0.5°	0.84	0.84	0.76	0.75
1.0°	0.82	0.81	0.78	0.78
2.0°	0.78	0.78	0.72	0.76

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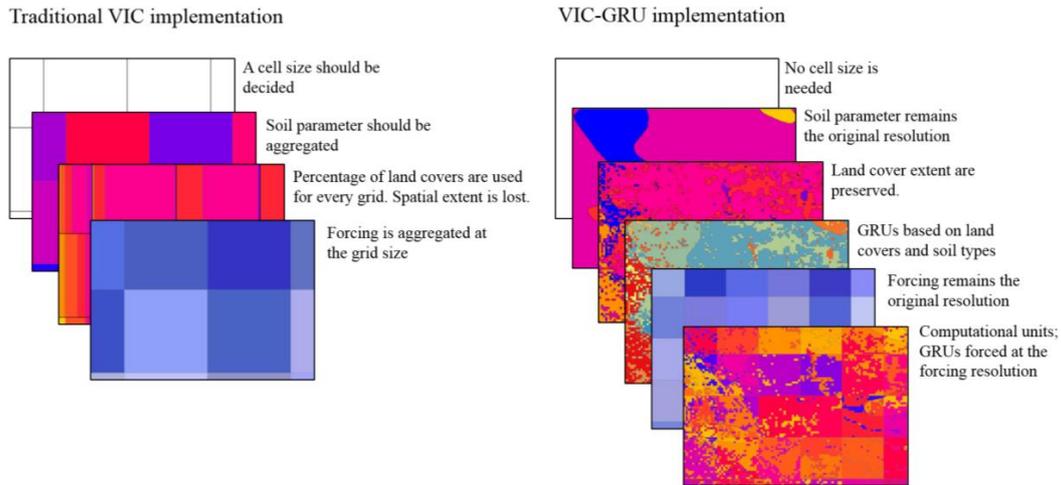
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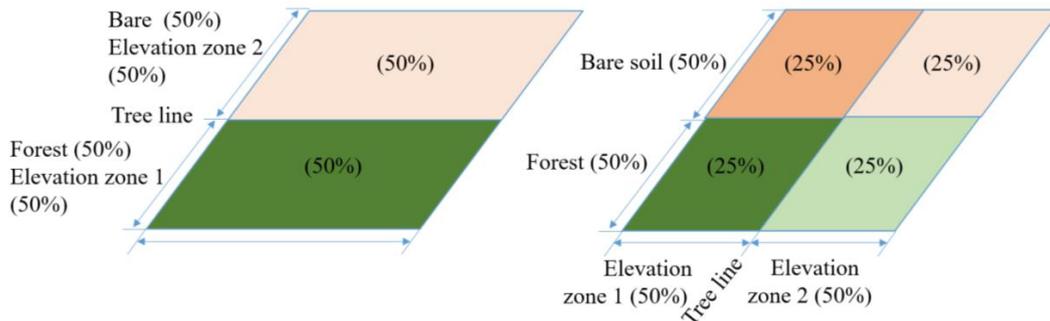
815 **10 Figures**



816

817 Figure-1- (a) Traditional VIC implementation and (b) new VIC implementation (VIC-GRU).

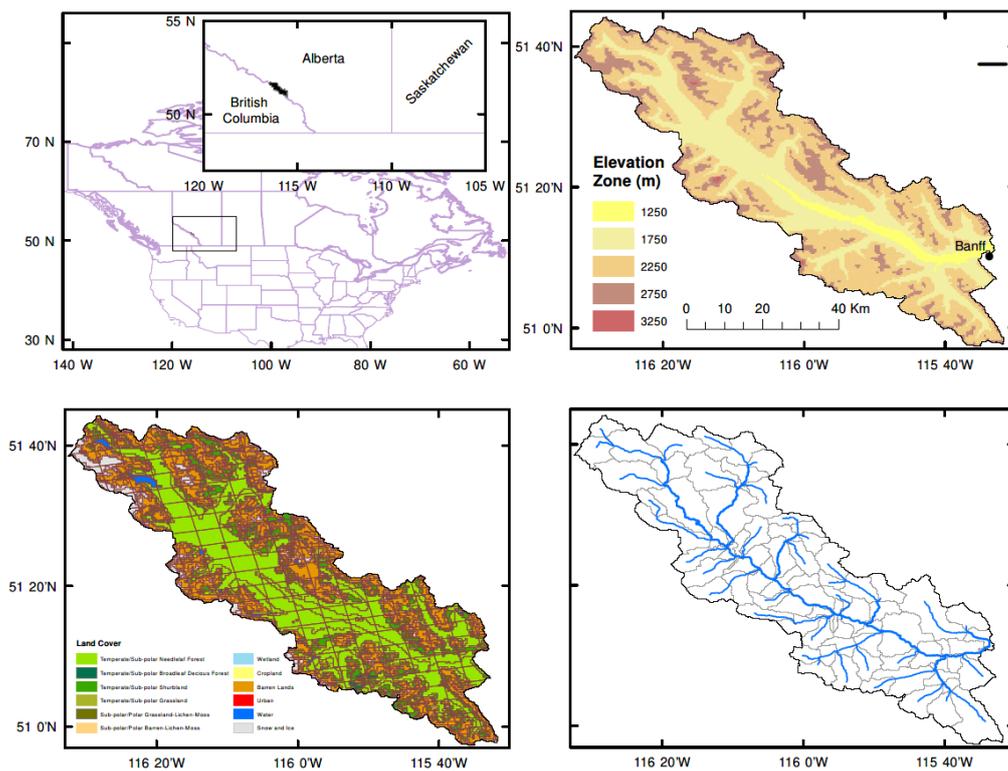
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820 Figure-2 – (Left) the true configuration of a natural system with land cover consist of 50% Bare
 821 soil and 50% forest within a grid located in two different elevation zones above and below the tree
 822 line and (right) the traditional VIC configurations for the given system at the grid for the two
 823 elevation zones and 2 land cover which results in unrealistic combination of forest cover above
 824 the tree line and bare soil below the tree line.

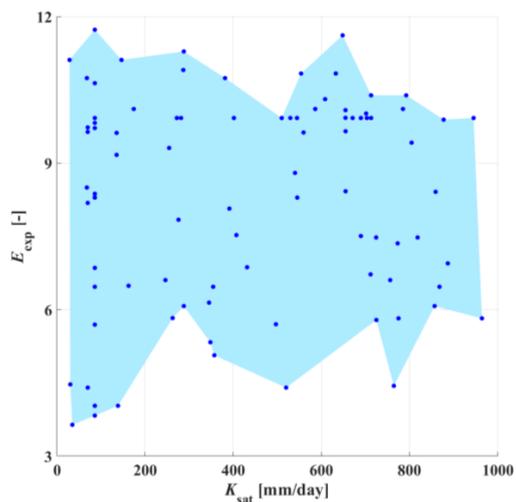
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827 Figure – 3 (a) The location of the Bow River Basin to Banff (b) GRUs for Case-3 color-coded for
828 elevation zones, (c) computational units for the Case-3-4km (Case-3 forced at forcing of 4 km
829 resolutions) and (d) river network topology and associated sub-basins for the vector-based routing.

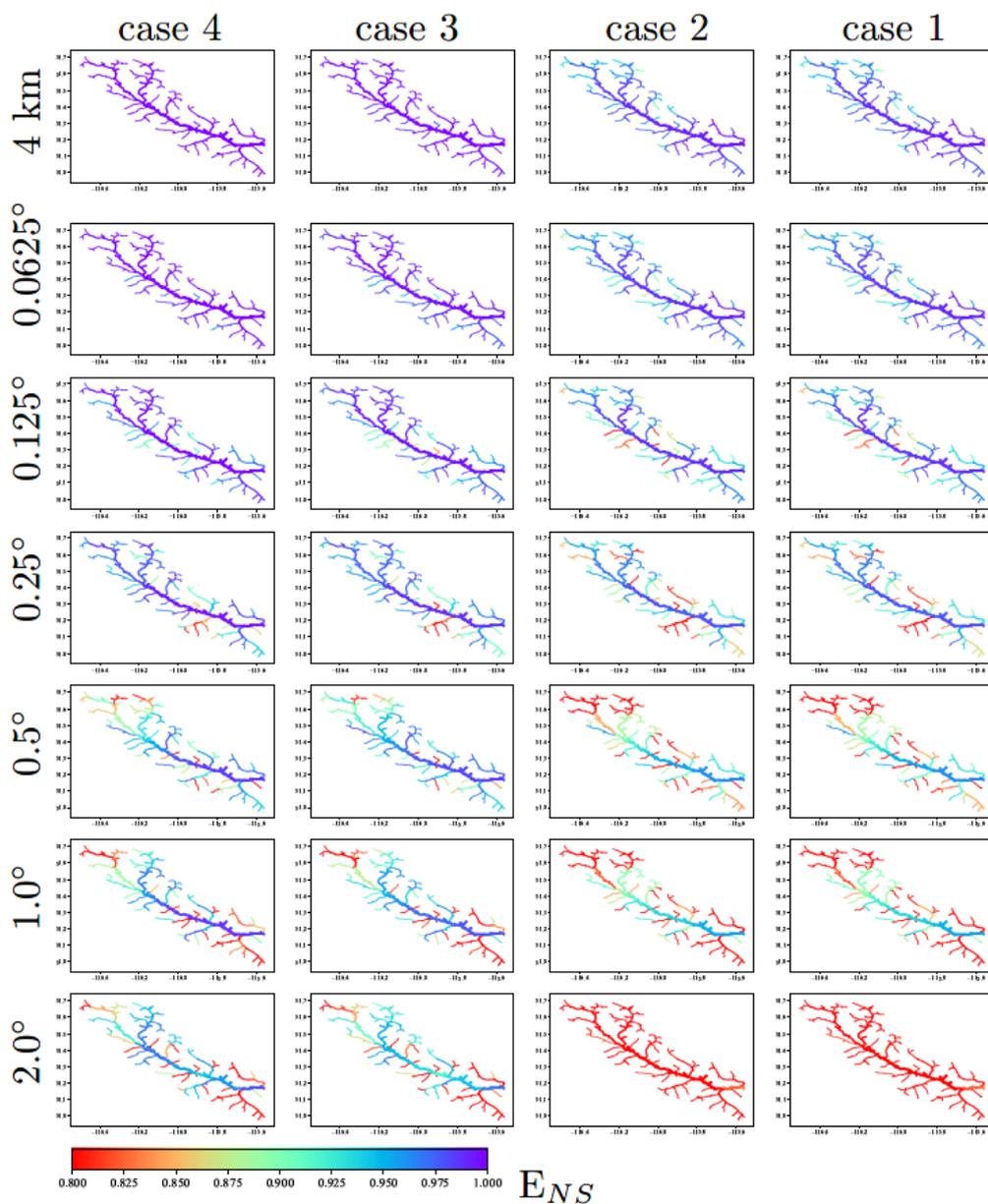
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832 Figure-4 – The spread of two parameters, saturated hydraulic conductivity, K_{sat} , and slope of water
833 retention curve, E_{exp} , for the parameters sets that have performance metric, E_{NS} , of more than 0.7
834 for configuration Case-2-4km. The axis are set to the ranges of the parameters.

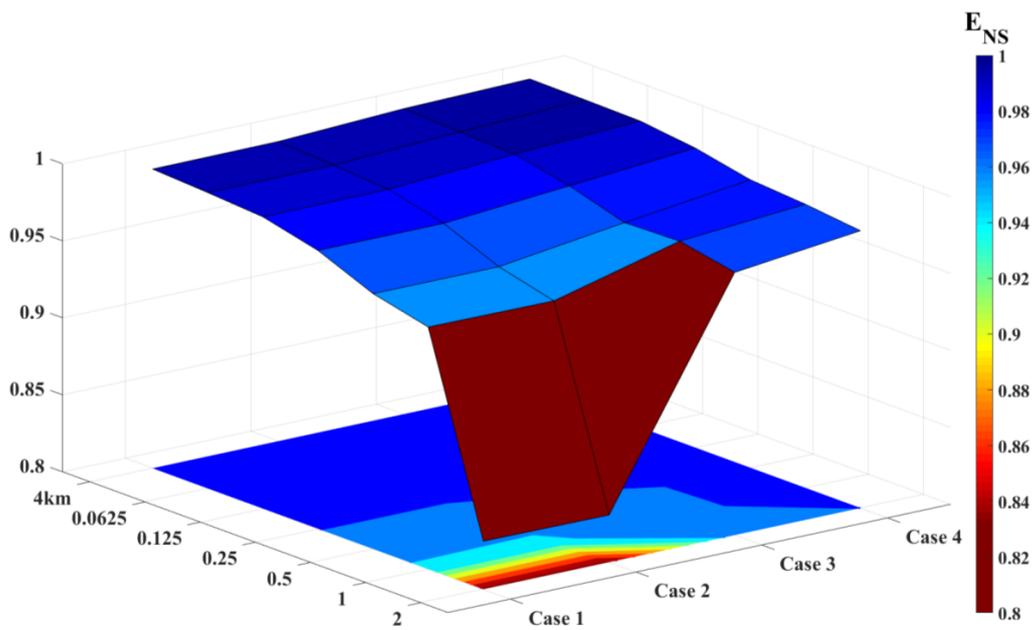
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837 Figure 5 – Deviation of the simulated streamflow at river segments in comparison with the
838 synthetic case of GRUs forced at 4km, Case-4-4km, expressed in performance metric, E_{NS} .

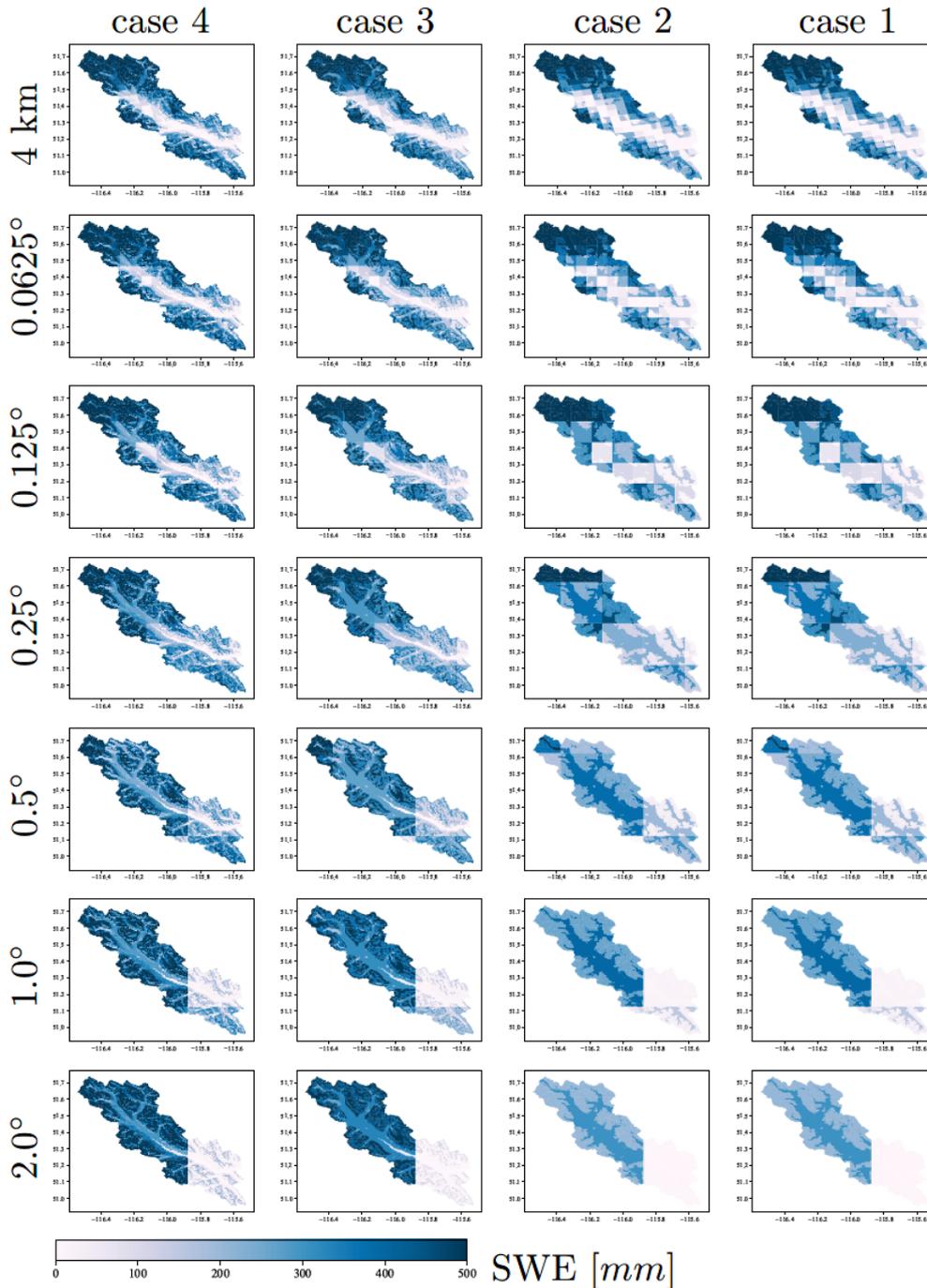
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841 Figure -6- The relative performance of model simulation across various configurations with a
842 single parameter set.

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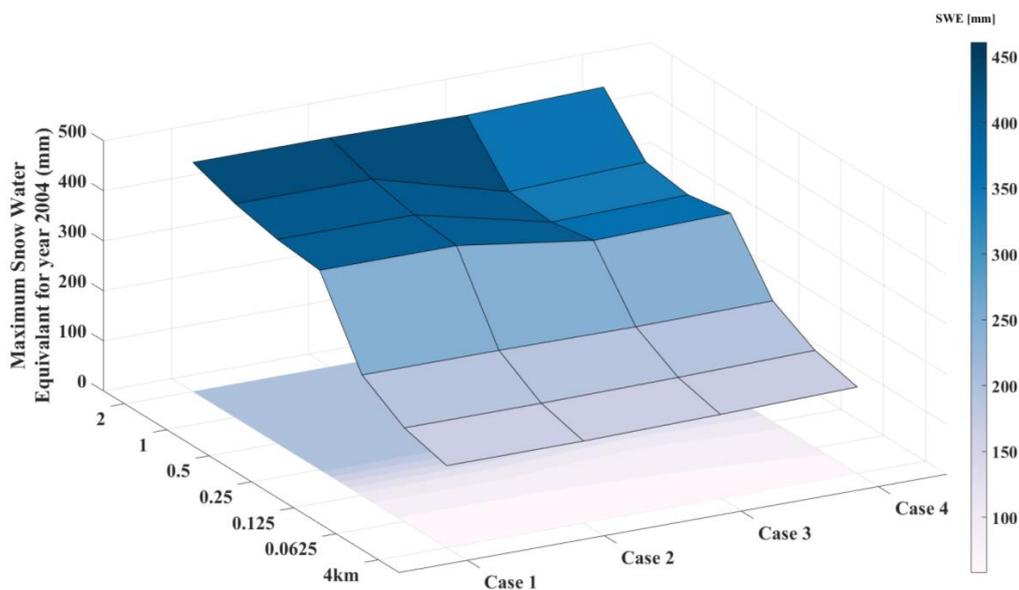


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845 Figure 7- Comparison of the snow water equivalent for 5th of May 2004 for various configurations.

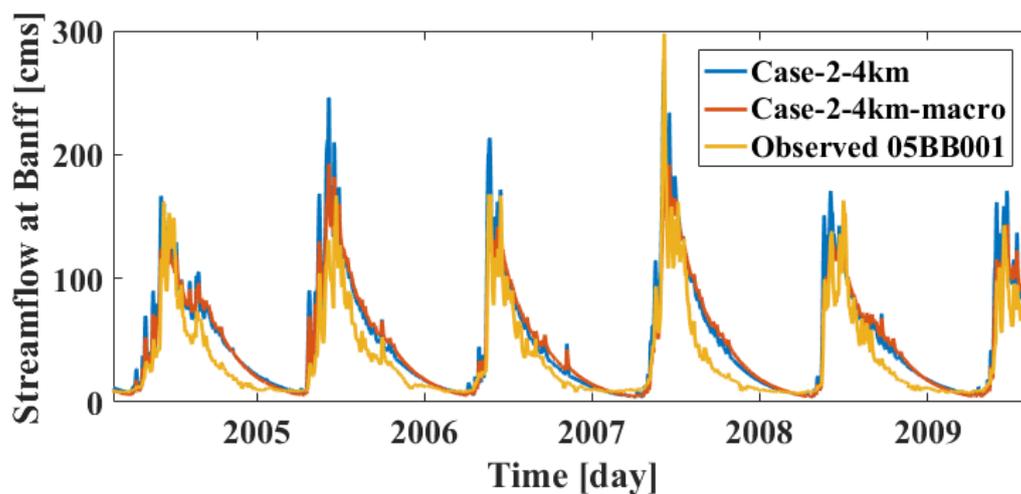


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848 Figure-8- Maximum of snow water equivalent for an arbitrary location of -116.134°W and
849 51.382°E located in Bow Valley Bottom across various model configurations for the year 2004.

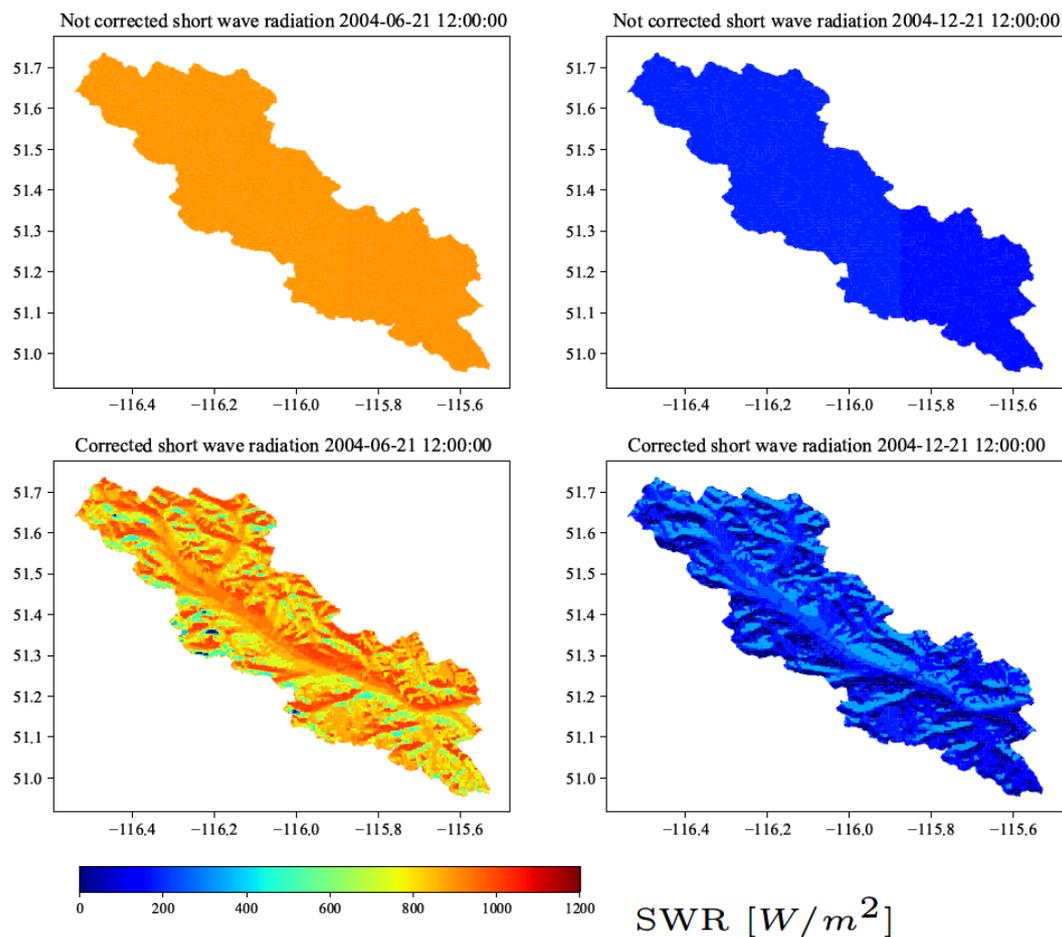


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851 Figure-9 comparison between the streamflow observation for Bow at Banff (05BB001) and model
852 with only micropore flow to slow reservoir, Case-2-4km, and only macropore to the slow reservoir,
853 Case-2-4km-macro.



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856 Figure A-1 Short wave radiation for (top left) not corrected for slope and aspect and (bottom left)
857 corrected for slope and aspect for 21st June 2020 and (top right) not corrected for slope and aspect
858 and (bottom right) corrected for slope and aspect for 21st December 2020.

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